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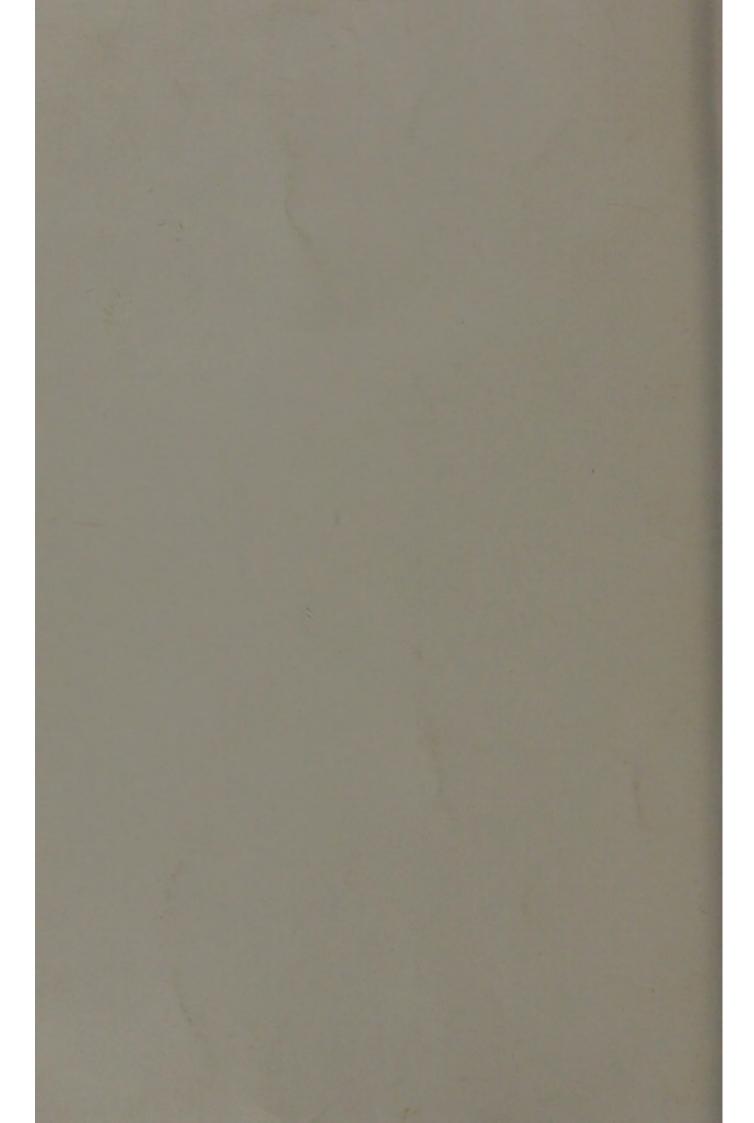
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HYGROMETRICAL TABLES

(14)

ADAPTED TO THE USE OF THE

DRY- AND WET-BULB THERMOMETER.

BY

JAMES GLAISHER, ESQ., F.R.S. &c.

FOURTH EDITION

LONDON:

TAYLOR AND FRANCIS, RED LION COURT, FLEET STREET.

1866.

HYGROMETRICAL TABLES

PREFACE

BUT NO REAL WAY OF SEPTIMENT

STEEL LAND WEIGHT STREET STREET

JAMES GLAISHER, 180, LEE &

PREFACE.

Many instruments have been constructed for the purpose of measuring the quantity of aqueous vapour in the atmosphere. Instruments used for this purpose are called *Hygrometers* (measurers of moisture), and have generally been made of substances which possess great capability for absorption, and undergo variation from that cause. Amongst hygrometrical substances may be reckoned cordage, catgut, wood (especially deal), the beard of the wild oat, &c. These in turn have all furnished material for the construction of Hygrometers, or rather Hygroscopes; but in use they are found to become less and less sensitive, and finally to lose all their hygrometrical properties.

Other substances have been sought for, which would regularly lengthen and shorten by the loss or absorption of moisture. Saussure of Geneva thought that this property might be found in a human hair, freed from all unctuosity by being boiled in a caustic ley. Thus prepared, he stretched and fastened it at one end to an easily moveable grooved wheel, with an index attached: whenever the hair was shortened or lengthened, the wheel and index were moved round, and thus indicated every increase or diminution of moisture.

M. De Luc constructed a hygrometer of a very thin piece of whalebone cut in a direction transverse to the fibre; this he affixed at one end by gold wire to a delicate wheel carrying an index, &c. The idea was suggested by the fact, that whalebone lengthens as it absorbs moisture, and shortens or contracts as it becomes dry. These two instruments are still in use on the continent; but confidence cannot be placed in their indications, nor in any which are dependent upon the hygrometric properties of any substance that has as yet been employed.

The Hygrometer invented by Mr. Daniell was a great advance upon the previous methods of construction. It denotes the degree of moisture in the air with considerable accuracy, exhibiting the amount in temperature of the dew-point, expressed in degrees of the ordinary thermometer, and thus

referred to a well-known standard of comparison.

The Hygrometer invented by M. Regnault is said to possess advantages over Daniell's Hygrometer, but in practice I have not found this to be the case. It consists of two delicate thermometers, kept in position by passing through corks fitting into long cylindrical cups of polished gold or silver, one of which is partly filled with ether, so that a portion of the bulb of its thermometer is immersed in it; a small tube passes through the corks, open at both ends, to which a flexible tube is fixed of any length, allowing the observer to be as distant from the instrument as he pleases; by this means air is drawn from or driven into the cups. The ether evaporates with a rapidity depending on the current, which is obtained at pleasure; dew is deposited on the cup containing the ether, the slightest dulling of which is seen by contrast with the other cup, which continues bright.

To use these instruments effectively, experience is required, united with a keen eye, and promptness of observation. Their employment is expensive, owing

to the required ether, which must be the best in quality and not sparingly supplied. It is difficult to procure good ether at all times; it suffers much loss from evaporation if kept or taken to hot climates, and deteriorates rapidly. When the air is very dry it is a long time before any deposition on the instrument takes place, and sometimes no deposit at all will ensue with bad or indifferent ether; neither are these instruments well adapted for observations at short intervals, as, from the principle of their construction, some little time must necessarily elapse before an observation can be repeated.

For these reasons, which forbid their general employment, I directed my attention some years ago to the most effective and simple method of determining the true hygrometric conditions of the air. This, I considered, would be best performed by the employment of the Dry- and Wet-bulb thermometers, which combined may be considered to constitute but one instrument, and to give results identical with Daniell's Hygrometer, over which they possess the advantage of requiring water only for their supply, and giving, when desired,

continuous observations.

The thermometers should have very small bulbs so as to be delicate and sensitive in the extreme; their graduations should be on their own stems, and their readings should be compared with those of a standard thermometer before use, to determine their index errors.

In my balloon experiments the temperature of the dew-point was determined at different heights by simultaneous readings of the Dry- and Wet-bulb ther-

mometers, Daniell's Hygrometer, and Regnault's Hygrometer.

In the experiments of every year there was not found any certain difference in the determination of the dew-point by Daniell's and Regnault's Hygrometers, and this temperature determined by the use of the Dry- and Wet-bulb thermometers, was found to be very closely approximate to the results obtained by either of the above instruments.

The results of all the simultaneous determinations of the temperature of the dew-point by Daniell's Hygrometer and the Dry- and Wet-bulb thermometers

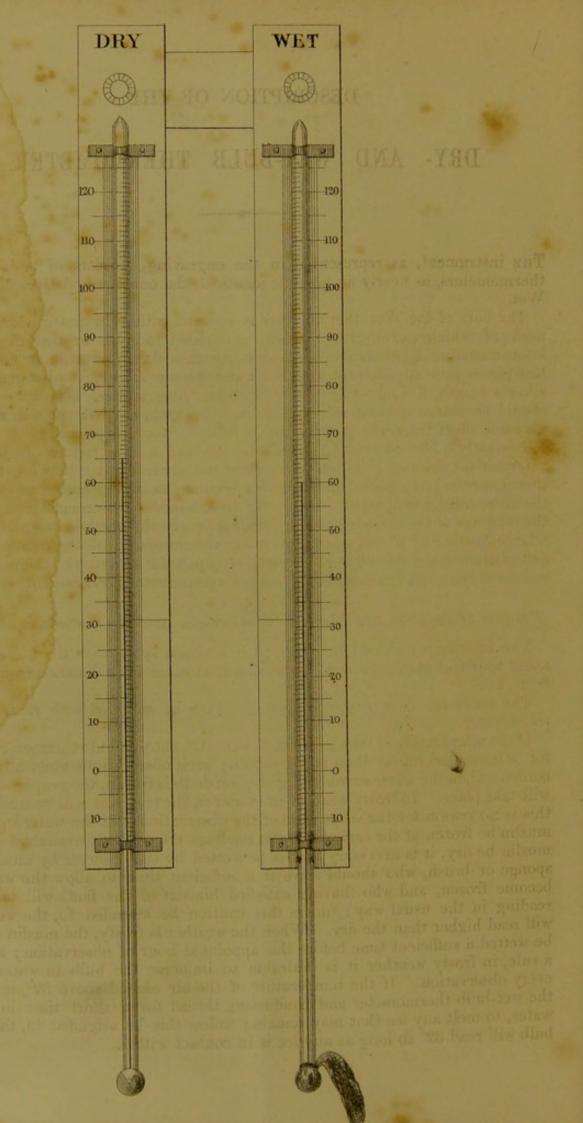
are as follows.

The temperature of the dew-point as found by the use of the Dry- and Wetbulb thermometers.

Up to	1,000 feet	t high was	0.15 lower	than by	Daniell's 1	Hygrometer,	from 28 exps.
From 1,000 to	2,000	"	0.10	1)	"	"	40
2,000 to	3,000	,,,	0.05	"	"	"	59
3,000 to	4,000 fee	t high was	s the same a	s by Dar	niell's Hyg	rometer	66
4,000 to		"	0.05 lower	"	"	"	40
5,000 to	6,000	,,	0.7	11	"	"	34
6,000 to	7,000	,,	0.2	"	"	"	34
7,000 to	8,000 fee	t high was	the same a	s by Dar	niell's Hyg	rometer	8
8,000 to		"	1.5 higher	"	"	11	2
9,000 to	10,000	"	1.2 higher		"	"	2
10,000 to	11,000	,,	0.3 higher	11	"	"	1
12,000 to	13,000	,,	0.3 higher	"	"	"	5
13,000 to	14,000	,,	0.8 lower	1)	"	"	7
14,000 to	15,000	"	1.0 lower	"	"	"	2

The number of experiments made up to the height of 7000 feet varying from 28 to 66 in each step of 1000 feet, are sufficient to enable us to speak with confidence; the results are that the temperatures of the dew-point, as found by the use of the Dry- and Wet-bulb thermometers and these Tables, are worthy of full confidence up to this point. At heights exceeding 7000 feet my experiments do not yield a sufficient number of simultaneous readings to give satisfactory results, and before we can speak with certainty at these high elevations more experiments must be made.

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DESCRIPTION OF THE

DRY- AND WET-BULB THERMOMETER.

THE instrument, as represented in the engraving, consists of two parallel thermometers, as nearly as possible identical, the one marked Dry, the other Wet.

The bulb of the Wet thermometer is covered with thin muslin, round the neck of which and over the muslin is twisted loosely, or tied in a loose knot, a conducting thread of lamp-wick, common darning cotton, or floss silk; this passes into an adjacent vessel of water placed at such a distance as to allow a length of conducting thread of about three inches. The cup or glass should be placed on one side and a little beneath, so that the water within

may not affect the reading of the dry bulb by its too near vicinity.

I greatly object to those instruments in which a long cistern of glass as a reservoir for the supply of water occupies the central space between the two thermometers; the water in the cistern becomes heated or cooled in excess of the surrounding temperature, and never fails, however imperceptibly, to vitiate the readings of the thermometer on either side. In this method of construction a large surface of metal is employed for the reception of the thermometers and cistern, and fails not to act injuriously upon the accuracy of the readings; nor do they in compensation offer a more symmetrical arrangement.

Position of the Dry- and Wet-bulb Thermometer, and Precautions in using it.

The instrument should be mounted in an open space with the bulbs raised about four feet above the soil, in the shade, at some little distance from walls, trees, &c.

The water-vessel or reservoir should always be supplied with rain or distilled water.

If the temperature of the air descend below 32°, the wet-bulb thermometer will for a time read higher than the dry-bulb; such observations must not be recorded: when the water surrounding the wet-bulb is frozen, the proper readings will take place. In frosty weather the water in the reservoir will be frozen, but this is no reason for the suspension of the observations; if the water upon the muslin be frozen at the same time, the readings are perfectly available. If the muslin be dry, it is necessary that it be wetted by the observer by means of a sponge or brush, who should leave it a sufficient time to allow the water to become frozen, and who (having satisfied himself of the fact) will take the reading in the usual way: unless this caution be attended to, the wet-bulb will read higher than the dry. When the weather is frosty, the muslin should be wetted a sufficient time before the appointed hour of observation; and, as a rule, in frosty weather it is desirable to immerse the bulb in water after every observation. If the temperature of the air ascend above 32°, immerse the wet-bulb thermometer and conducting thread for a short time in warm water, to melt any ice that may remain; unless this be attended to, the wetbulb will read 32° so long as any ice is in contact with it.

Before use, the cotton lamp-wick should be washed in a solution of carbonate of soda, and pressed whilst under water throughout its length. In use it should be of such extent that the water conveyed be sufficient in quantity to keep the muslin on the bulb as moist as when the air is saturated with vapour. The amount of water supplied can be increased or diminished by increasing or decreasing the extent of the conducting thread.

In observing, the eye should be placed on a level with the top of the mercury in the tube; and the observer should be careful to refrain from breathing

whilst taking the observation.

Temperatures of the Air and of Evaporation

are given by the readings of the two thermometers.

Temperature of the Dew-Point

If a mass of air be gradually cooled, it will descend to a degree of temperature at which it will be saturated by the quantity of vapour then mixed with it. This temperature is called the dew-point. It can be found directly from observation by the use of either Daniell's or Regnault's Hygrometer.

Calculating the Dew-Point from observations of the Dry- and Wet-bulb Thermometers.

Table I.—Factors by which it is necessary to multiply the excess of the reading of the dry thermometer over that of the wet, to give the excess of the temperature of the air above that of the Dew-Point, for every degree of air-temperature, from 10° to 100°.

Reading of Dry-bulb Therm.	Factor.	Reading ofDry-bulb Therm.	Factor.	Reading of Dry-bulb Therm.	Factor.	Reading ofDry-bulb Therm.	Factor.
10 11 12 13 14 15 16 17 18 19 20 21 22 23 24 25 26 27 28 29 30 31 32	8.78 8.78 8.78 8.77 8.76 8.75 8.70 8.62 8.50 8.34 8.14 7.88 7.60 7.28 6.92 6.53 6.08 5.61 5.12 4.63 4.15 3.70 3.32	33 34 35 36 37 38 39 40 41 42 43 44 45 46 47 48 49 50 51 52 53 54 55	3'01 2'77 2'60 2'50 2'42 2'36 2'32 2'29 2'26 2'23 2'20 2'18 2'14 2'12 2'10 2'08 2'04 2'04 2'04 2'04	56 57 58 59 60 61 62 63 64 65 66 67 68 69 70 71 72 73 74 75 76 77 78	1'94 1'92 1'90 1'89 1'88 1'87 1'86 1'85 1'82 1'81 1'80 1'79 1'78 1'77 1'76 1'75 1'74 1'73 1'72 1'71	979 80 81 82 83 84 85 86 87 88 89 90 91 92 93 94 95 96 97 98 99 100	1.69 1.68 1.67 1.67 1.66 1.65 1.65 1.64 1.63 1.62 1.62 1.60 1.59 1.59 1.58 1.58

The numbers in this Table have been found from the combination of all the simultaneous observations of the dry- and wet-bulb thermometers with Daniell's Hygrometer, taken at the Royal Observatory, Greenwich, from the year 1841 to 1854, with some observations taken at high temperatures in India, and others at low and medium temperatures at Toronto. The results

at the same temperatures were found to be alike at these different places;

and therefore the factors may be considered as of general application.

By the numbers in this Table the temperatures of the dew-point in the general tables have been calculated; and these have been constantly checked by direct observations with Daniell's Hygrometer, at the Royal Observatory, Greenwich, till the present time, 1866.

Expansion of Air from Heat.

M. Regnault has determined that air expands $\frac{1}{491\cdot13}$ part for every increase of one 1° of heat. The following Table has been calculated using this value, considering a volume of air under the pressure of 30 inches of mercury and at the temperature of 32° as the unit of comparison.

Table II.—Showing the volume of a mass of Dry Air after expansion from heat, for every degree of Fahrenheit's scale, from 0° to 100°.

Temp. Fahr.	The volume after expansion from heat.	Temp. Fahr.	The volume after expansion from heat.	Temp. Fahr.	The volume after expansion from heat.
0 0	0.9348448	34	1'0040722	68	1.0732996
1	9368809	35	.0061083	69	0753357
2	9389170	36	'0081444	70	.0773718
3	9409531	37	*0101805	71	'0794079
4	9429892	38	'0122166	72	.0814440
5	9450253	39	*0142527	73	.0834801
5	9470614	40	0162888	74	'0855162
7	9490975	41	'0183249	75	.0875523
7 8	9511336	42	0203610	76	*0895884
9	9531697	43	*0223971	77	*0916245
10	*9552058	44	'0244332	78	*0936606
11	9572419	45	0264693	79	*0956967
12	9592780	46	0285054	80	*0977328
13	*9613141	47	'0305415	81	*0997689
14	9633502	48	*0325776	82	.1018020
15	9653863	49	'0346137	83	1038411
16	9674224	50	0366498	84	1058772
17	9694585	51	.0386859	85	1079133
18	*9714946	52	'0407220	86	1099494
19	9735397	53	0427581	87	.1119852
20	*9755668	54	'0447942	88	1140216
21	9776029	55	.0468303	89	1160577
22	9796390	56	.0488664	90	.1180938
23	9816751	57	.0509025	91	1201299
24	*9837112	58	'0529386	92	1221660
25	'9857473	59	.0549747	93	1242021
26	9877834	60	.0570108	94	1262382
27	.9898195	61	.0590469	95	1282743
28	9918556	62	.0610830	96	*1303104
29	9938917	63	.0631191	97	1323465
30	9959278	64	'0651552	98	*1343826
31	0.9979639	65	.0671913	99	1364187
32	1,0000000	66	.0692274	100	1.1384248
33	1.0050391	67	1'0712635	100	

Elastic Force of Aqueous Vapour.

M. Regnault has determined, by a very careful series of experiments, the value of the Elastic Force of Vapour (Annales de Chimie et de Physique, 3° série, tom. xv.). The numbers in the following Table have been calculated from his results.

Table III.—Showing the Elastic Force of Aqueous Vapour, in inches of Mercury, from -41° to 100°, calculated from the experiments of Regnault.

Temp.	Force of	Temp.	Force of	Temp.	Force of	Temp.	Force of	Temp.	Force of
Fahr.	Vapour.	Fahr.	Vapour.	Fahr.	Vapour.	Fahr.	Vapour.	Fahr.	Vapour.
0	in.		in.		in.	0	in.	0.451	in.
-41'0	0.002	6.1	0.024	12'2	0.072	18.3	0.000	24'4	0.131
-40.0	1005	'2	*057	*3	.075	14	,100	.5	*132
-38.0	*006	*3	.028	*4	·075	.6	.101	•6	.133
-37'0	*006	- 5	.028	•6	.076	.7	.101	.8	*133 *134
-36.0	*007	.6	.059		*077	.8	102	.9	*134
-350	*007	·7 -8	'059	*7	*077	.9	102	25'0	135
-34.0	*007	1777.0	*059	.9	*077	19'0	*103	·1	*136
-33.0	*008	.9	.059	13.0	.078	.I	-103	.2	.136
-32'0	*008	7.0	*060	'I	*078	'2	*104	.3	137
-30.0	1009	'1 '2	*060	*3	*079	·3 ·4	104	*4	*137
-290	.010	•3	-060	*4	079	•5	105	.6	.139
-280	.010	.4	.060		*080	.6	.106	.7	.139
-27'0	110.	*5	.061	.6	*080	.7	.106	-8	140
-26.0	110.	.6	.061	•7	.081	-8	107	.9	140
-25.0	*012	.7	.061	.8	.081	.9	107	26.0	141
-24'0	'013	-8	•061	.9	.081	20'0	.108	.1	*142
-23'0	*014	.9	*062	14'0	*082	.1	.108	*2	142
-21.0	016	8.0	*062 *062	'I	*082	*2	.109	*3	143
-20'0	'017	.2	*062	•3	.083	·3 ·4	.110	•5	·143
-19.0	*017	•3	.063	*4	.083	•5	.110	.6	145
-18.0	.018	.4	.063		.084	.6	III.	-7	*145
-17.0	*019		*063	.6	.084	•7	·III	-8	*146
-16.0	'020	.6	*063	.7	*085	-8	112	.9	*146
-150	*021	.7	*064	The second second	*085	.9	*112	27.0	*147
-14.0	'022	-8	*064	.9	.085	21'0	.113	.I	*148
-13.0	'023	.9	.064	15.0	*086	.I	.113	.2	*148
-11.0	'024	9.0	·065	'1 '2	-086 -086	*2	114	•3	*149
-10.0	025	'I	-065	*3	*087	·3 ·4	114	•5	*150
- 0.0	028	-3	•066	*4	*087	•5	-115	.6	151
- 8.0	*029	.4	•066		*088	.6	.116	.7	*151
- 7'0	*031		•066	.6	.088	•7	•116	-8	152
- 6.0	'032	.6	•066	·7 -8	*089	-8	*117	.9	*152
- 5.5	*033	.7	.067	0.00	*089	.9	-117	28.0	*153
- 5.0	*034	.8	.067	.9	.089	22'0	.118	·1	154
- 4.5	.035	.9	*067	16.0	.000	I.	.118	*2	154
- 4.0	'036	10.0	·068	·1	.090	'2	.119	.4	.122
- 3.0 - 3.2	·037	'1 '2	•068	•3	.090	·3 ·4	119		*156
- 2.2	.039		•069	*4	.091		120	•6	*157
- 2'0	'040	*3	•069	.5	1092	.6	121	.7	.128
- 1.5	'041	-5	*069	.6	*092	·7 ·8	121		.128
- 1.0	'042	.5	*069	.7	.093		122	.9	.159
- 0.2	'043	.7	*070		*093	.9	122	29.0	.160
0.0	.044		*070	.9	. *093	23'0	123	·1	.161
+ 0.2	*045	.9	*070	17'0	*094	I.	124	.3	162
1.2	°046	11.0	·071	'I	*094	.2	124	*4	.162
2.0	.048	.2	.071	•3	*095	*3 *4	125	.5	•163
2.2	.049	•3	*072	.4	*095	*5	126	•6	.164
3.0	.050	*4	*072	.5	*096	*5	127	*7	-165
3.2	.021	•5	*072		-096	·7 ·8	127	111 177	•166
4.0	'052		*072	.7	*097		.128	*9	·166
4.5	.023	.7	.073		-097	.9	.128	30.0	•168
5.0	*054		*073	9	1097	24.0	*129	*2	•168
5'3	*055	12.0	*073	18.0	.098	'I	.130 .	•3	•169
5'7 6'0	0.024	12'1	0'074	18.2	0,099	24.3	0,131	30'4	0'170
	31		11		99	1.3		THE RESERVE OF THE PERSON NAMED IN	

TABLE III. (continued).

	mehes	ni m	Vapor	Aqueous	10 99	nod nor	until 90	T MULLING	MC-+T	lak iller
-	Temp. Fahr.	Force of Vapour.	Temp. Fahr.	Force of Vapour.						
1	0	in.	0	in.	0	in.	0	in.	0	in.
-	30.2	0'170	37'0	0'220	43.5	0'283	50'0	0'361	56.5	0.457
1	6	171	'2	'221	16	284	I.	*362	.6	459 461
-	.7	172	'3	222	.7	°285	'2	*364 *365	.7	462
	.9	173	-4	224	'9	287	-4	*366	.9	*464
1	31.0	174	.6	*225	44'0	*288	.5	367	57.0	*465
	11	174		'225	I	'289	THE RESERVE	.369	T.	*467
	12	175	.7	226	'2	290	.7	370	.2	469
	·3 ·4	176	.9	1227	'3 '4	292	.9	371	·3 ·4	'470 '472
	.5	177	38.0	'229	.5	*294	51.0	374		'473
		178	I.	'230	.6	*295	.I	375	.6	475
	.7	179	.2	'231	'7	- 296	'2	377	.7	'477
	.9	180	:3	231	.8	297	3	'378	THE RESERVE TO SECURITY OF THE PARTY OF THE	'479 '480
-	32'0	.181	*4	232	45.0	298	*4	·379 ·381	58.0	482
	.I	182	.6	234	1,	.301	.6	382	.1	.483
	'2	.185	.7	'235	'2	'302	·7 -8	*384	'2	'485
	3	.183		'236	*3	.303		.385	13	*487
1	4	184	39.0	237	*4	304	.9	·386 ·388	-4	.489
	.6	185	390	238	.6	305	52.0	-389	.5	'491 '492
	·7 ·8	.186	'2	*239	-7	307	'2	.391	.7	494
		.186	*3	*240	-8	.308	.3	393	-8	'496
	.9	187	-4	'241	.9	'309	.4	394	.9	498
	33.0	.188	.5	242	46.0	311	.6	*396	20.0	1500
1	.2	.180	-7	244	.2	313	-7	397	.2	·503
	-3	190	-8	245	-3	'315	.8	400	-3	.202
	4	161.	.9	'246	-4	.316	-9	'401	-4	.507
1	.5	192	40.0	247	.6	'317	53.0	'403	.5	.209
	.7	.193	'I	*248	.7	.318	.1 .5	*404 *406	·6	.211
	.8	194	.3	250	-8	321	.3	407	-8	*512 *514
	.9	195	-4	'251	-9	.322	•4	*409	.9	-516
1	34'0	.196	.5	'252	47'0	'323	.5	'410	60.0	.218
	I.	.196		253	I.	324		'412	I.	*520
	.2	197	.7	254	.3	'325 '327	·7 -8	'413	.2	*522
	·3 ·4	.199	.9	256	.4	328	.9	'415 '416	*3 *4	524
	-5	.199	41'0	*257	*5	.329	54.0	*418	-5	.528
		'200	.I	*258		.330	.I	*419	-5	.529
	.7	201	.2	*259 *260	7 -8	.331	'2	'42 I	.7	.231
	.9	203	·3 ·4	*261	.9	333	·3 ·4	'422 '424		533
	35'0	*204	.5	'262	48.0	335	.5	425	61.0	*535 *537
Т	.I	*204	.6	*263	.I	*336	.6	'427	.I	-539
1	'2	205	.7	*264	'2	.338	·7 -8	'428	'2	541
	·3 ·4	'206 '207	.0	*265	·3 ·4	339		'430	·3 ·4	543
	.5	208	42.0	267	.5	340	55.0	'431 '433	4	545
1	.6	*208	I.	*268	.6	343	.1	434	.5	·546 ·548
	.7	209	'2	269	.7	*344	.2	436	·7 ·8	.550
		210	3	270		345	13	'437		*550 *552
1	36.0	212	**	271	49'0	·346 ·348	·4	439	6.9	554
1	.I	213	.6	273	17	349	.6	441	62.0	556
1	'2	214	.7	*274	12	.321	.7	444	-2	*558 *560
	-3	214		275	.3	352	.8	'446	.3	·560 ·562
	*4	215	43'0	276	:4	353	-6.9	'447	4	*564
1	.5	217	430	277	.6	355	26.0	449	.5	-566
	.7	'218	.2	279		357	.2	453		.568
1		'218	3	280	.8	357	.3	454	.7	570
1	36.9	0'219	43'4	0'281	49'9	0.360	56.4	0.456	62.9	0.574
-	-	1	The same	and the same of	and the same				1	

Table III. (continued).

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Temp. Fahr.	Force of Vapour.	Temp. Fahr.	Force of Vapour.	Temp. Fahr.	Force of Vapour.	Temp. Fahr.	Force of Vapour.	Temp. Fahr.	Force of Vapour.
0	in.	0	in.	9	in.	0	in.	_ 0	in.
63.0	0.246	69.5	0.471	76.0	0.897	82.2	1.110	89.0	1.366
I.	1578		723	.1 .7	.900	.6	114	1	370
'2	'580 '582	.7	726	.3	1903	.7	117	'2	375
.4	.584	.9	731	-4	.909	.9	124	·3 ·4	'379 '384
	.586	70'0	733	15	912	83.0	128	.5	-388
.6	.588	I.	'736	.6	.915	.I	.131	.6	393
.7	'590	'2	.738	.7	.918	'2	.132	.7	397
	592	3	*741		921	:3	,139		.401
69	594	. 4	744	.9	'924	-4	142	.9	'406
64.0	·598	.6	746	77.0	*930	.6	146	30.0	'410
'2	.601		751	'2	934	.7	154	'2	'415 '419
.3	.603	.7	754	.3	937	-8	157	.3	424
'4	.605	.9	.756	-4	.940	.9	.191	.4	'428
.5	.607	71'0	759	.6	'943	84.0	165	.6	'433
	.609	I.	'761		946	.1	.169		'437
.7	611	.2	·764 ·766	.7	949	'2	173	.7	'442
.9	615	·3 ·4	769	.9	952	·3 ·4	.180	.9	'446 '451
65.0	.617		772	78.0	958		184	91.0	455
.1.	'620	.6	.774	.1	*961	.6	.188	I.	*460
. '2	.622	.7	.777	'2	965	.7	192	'2	464
'3	'624	.8	'779	.3	.968	CANAL CANAL	.196	'3	'469
-4	626	.9	782	- 4	'971	9	'200	- '4	'473
.6	·628 ·630	72.0	785	.5	974	85.0	1203	.5	'478 '483
	-633	'2	.790		977	'2	'211		487
.7	-635	.3	1793	.7	.984	.3	'215	.7	492
.9	.637	.4	.796	.9	.987	-4	'219	.9	-496
66.0	.639	.5	'799	79'0	.990	.5	'222	92.0	.201
I.	.641		.801	.I	'994		*226	I.	.202
'2	.644	.7	*804	*2	0.997	.7	230	'2	.210
:3	·646 ·648	195	·807 ·810	.3	1,000	.9	234	·3 ·4	.215
.4	.650	73.0	.812	.4	'003	86.0	242		519
.6	.652	1,20	.815	.5	.010	.1	*246	.5	529
The Control of the Co	.655	'2	-818	.7	'013	'2	250.	.7	1534
.8	·657 ·659	·3 ·4	. 820	1000	.016	·3 ·4	254		-538
67.0	.659	'4	-823	6.0	*020	-4	*258	.9	543
67.0	.661	.5	·826 ·829	80.0	1023	.6	·262 ·266	93.0	'548
.1	·664 ·666		-832	.2	.030		270	'2	*553 *557
.3	-668	.7	-834		.033	.7	274	.3	1562
.4	.671		-837	·3 ·4	.037	87.0	278	4	.567
.5	.673	74.0	·837 ·840 ·843	.5	'040		282	.6	572
	.675	'I	.843		*043	I.	*286		*577
-7	.678	'2	*846	.7	*047	.2	1290	7.8	.581
	·680 ·682	3	*848	.9	050	·3 ·4	*295 *299	.9	·586
68.0	-684	.4	·851 ·854	81.0	'057	.5	.303	94.0	-596
.1	-687	.5	*857	I.	*060	.5	*307	I.	.601
'2	.689	7 -8	*860	'2	*064	.7	.311	'2	*606
.3	.692		-863	.3	*067		.312	3	'611
1 4	·694 ·697	.9	.865	4	.070	88.0	.319	. 4	.616
.5	1697	75.0	·868 ·871	.5	*074	88.0	323	.5	621
0	·699	'2	874		'077 '081	1 2	-328 -332		631
.7	704	.2	-877	.7	-084	.3	336	7 .8	-636
	.706	·3 ·4	.880	.0	.088	4	*340	6.	·641
69.0	.708	.5	-883	82.0	*092	.5	345	95.0	.646
I.	'711		-885	I.	*095		349	I.	.651
'2	'713	.7	-888	'2	.099	.7	353	.3	·657 ·662
60.4	716	100000000000000000000000000000000000000	0.894	82.4	1.100	88.9	1.361	95.4	1.667
69.4	0.718	75'9	0 894	024	1.00	409	1 . 200	754	
1	-	Management	1	-	-	-			

Table III. (continued) . .

Temp. Fahr.	Force of Vapour.	Temp. Fahr.	Force o Vapour						
0	in. 1.672	96.5	in.	0	in.	98.5	in. 1.833	in. 99°5	in. 1.890
95.5	677	9.6	730	97.5	784	9.6	-839	99.5	-896
.7	.682	·7 ·8	*735	.7	790	. '7	*845	'7	.901
-8	.687		741	-8	795	-8	.850	.8	*907
.9	*692	.9	746	.9	.801	.9	.856	.9	912
96.0	-697	97'0	751	98.0	.806	99.0	.862	100.0	.918
.I	*703	.I	757	I.	-811	I.	-868	.I	923
'2	*708	'2	762	.2	*817	- 12	873	'2	929
'3	714	.3	.768	*3	-822	*3	*879	.3	'935
96.4	1.719	97.4	1.773	98.4	1.828	99'4	1.884	100'4	1'940

From the numbers in this Table the Elastic Force of Vapour in the General Tables have been found.

The numbers in this Table show the length of a column of mercury, corresponding to the pressure of aqueous vapour at different temperatures. As in an atmosphere of pure steam its force at the earth's surface is its weight, so in a mixture of atmospheres, the elastic force of each at the surface of the earth is the weight of each. Therefore the elastic force of aqueous vapour representing the weight of the entire mass diffused throughout the atmosphere expresses the pressure on the surface in the cistern of the barometer, produced by the vapour present at the time of observation. To find the elastic force of vapour at any time, it is simply necessary to determine the temperature of the dew-point, and to seek for that temperature in this Table, and the quantity of vapour which corresponds to it is seen by inspection.

For instance, suppose the temperature of the dew-point be 51°, opposite to this reading in the Table is 0.374 inch of mercury, a quantity which is about

 $\frac{1}{80}$ th part of an atmosphere whose whole pressure is 30 inches.

As the pressure of the whole atmosphere is about 15 lbs. on the square inch when the reading of the barometer is about 30 inches, and as the weight of vapour in the atmosphere when the temperature of the dew-point is 51° is about $\frac{1}{80}$ th part of the whole pressure, it follows that the actual weight of the vapour is about $\frac{15}{80}$ lb., or 1300 grains nearly. The weight of a cubic inch of water is 253 grains; therefore the quantity of water present in a column of the atmosphere reaching to its limit is $\frac{1300}{253}$, or about 5 inches.

An examination of the numbers in this Table at different temperatures shows that the increased capacity of heat for aqueous vapour at higher temperatures does not follow the same ratio as the temperature, the capacity for aqueous vapour at any temperature being less than the mean of equidistant temperatures: for example, at 50° the elastic force of vapour is 0.361 inch, and at 70° is 0.733 inch; if, therefore, two masses of air, the one at 50° and the other at 70° (both being saturated with moisture), be mixed together, the compound will take a mean temperature of 60°; but the elastic force of vapour at 60° is 0.518 inch, while the mean of the forces at 50° and 70° is 0.547. The tension of vapour is therefore greater than the air can sustain, and the excess must fall.

Weight of a Cubic Foot of Air.

From M. Regnault's experiments, 1000 cubic inches of dry air under the pressure of 30 inches of mercury, and at the temperature of 60°, weigh 310·3529 grains, and 1000 cubic inches of water under the same pressure,

and at the same temperature, weigh 252525 grains; therefore water is 813.67 times heavier than air.

From Table II., the volume of a mass of dry air at 60°, whose volume at 32° is represented by unity, is 1.05701.

Therefore the weight of a cubic foot of dry air at 32° is equal to the weight

at 60°, viz. 536.3 grains, multiplied by 1.05701, or to 566.86 grains.

The following Table has been calculated by dividing 566.86 by the number expressing the volume of dry air after expansion from heat, as contained in Table II.

TABLE IV .- Showing the weight in Grains of a Cubic Foot of Dry Air, under the pressure of 30 inches of Mercury, for every degree from 0° to 10000 ⋅

Temp. Fahr.	Weight of a Cubic Foot of Dry Air.	Temp. Fahr.	Weight of a Cubic Foot of Dry Air.	Temp. Fahr.	Weight of a Cubic Foot of Dry Air.	Temp. Fahr.	Weight of a Cubic Foot of Dry Air.
0	grs.	26	grs.		grs.	0	grs.
0	606.37		573.87	51	545'74	76	520'25
2	605.05	27	572.69	52	544'67	77	519.28
777	603.74	1000	571.21	53	543.61	78	218.31
3	602'43	29	570'34	54	542'55	79	517.35
4	601.13	30	569.17	55	541.20	80	516.39
5	599.83	31	568-o1	56	540'45	81	515'43
	598.54	32	566.85	57	539'40	82	514.48
7 8	597'26	33	565.70	58	538.36	83	513.23
	595.98	34	564.56	59	537'32	84	512.59
9	594.71	35	563.42	60	536.58	85	511.65
10	593'44	36	562.28	61	535'25	86	510.41
II	592.18	37	561.12	62	534'22	87	509.77
12	590.92	38	560.02	63	533'20	88	508.84
13	589.67	39	558.89	64	532.18	89	507.91
14	588.42	40	557'77	65	531.12	90	506.99
15	587.18	41	556.66	66	530.16	91	506.07
16	585.95	42	555'55	67	529.15	92	505'15
17	584.72	43	554.44	68	528'14	93	504'23
18	583'49	44	553'34	69	527'14	94	503.35
19	582.27	45	552'24	70	526.12	95	502'41
20	581.05	46	551'15	71	525.16	96	501.20
21	579.84	47	550.06	72	524'17	97	500.60
22	578.64	48	548.97	73	523.18	98	49970
23	577.44	49	547.89	74	522'20	99	498.81
24	576.24	50	546.82	75	521'22	100	497'93
25	575'05	41111					The state of the state of

Enlargement of Volume of Air by Vapour.

If a volume of dry air of known elasticity be mixed with an equal volume of vapour, also of known elasticity, and if the mixture be so compressed as to occupy a space only equal to one of these volumes, the elasticity of the mixture will be the sum of the two elasticities of the air and vapour; or if the mixture be allowed to expand till its elasticity is equal to that of the unmixed air, it will occupy a larger volume in the proportion of the sum of the two elasticities to the elasticity of the air alone.

Let p=the atmospheric pressure as measured by inches of mercury in the barometer tube.

 E_t =the elastic force of vapour at temperature t measured in inches of mercury in the barometer tube.

n=the bulk of a certain quantity of air, when dry, at the temperature

t, and under the pressure p.

Let n' = the bulk of the same quantity of air when saturated with vapour, at the temperature t, and under the pressure p.

The elasticity varies inversely as the volume, the temperature remaining the same; therefore that portion of the elastic force p, which depends on the air only which occupies the space $n' = \frac{np}{n'}$,

and the whole atmospheric pressure

$$p = \frac{pn}{n'} + E_t,$$
or
$$\frac{n}{n'} = \frac{p - E_t}{p},$$

$$= 1 - \frac{E_t}{p};$$

$$\therefore n' = \frac{n}{1 - \frac{E_t}{p}}.$$

And from this formula the following Table has been constructed :-

Table V.—Showing the enlargement which a volume of Dry Air receives when saturated with Vapour under the pressure of 30 inches of Mercury, for every degree of temperature, from 0° to 100°.

Temp. Fahr.	Increased volume owing to the pre- sence of vapour, the original bulk being considered as unity,	Temp. Fahr.	Increased volume owing to the pre- sence of vapour, the original bulk being considered as unity.	Temp. Fahr.	Increased volume owing to the pre- sence of vapour, the original bulk being considered as unity.	Temp. Fahr.	Increased volum- owing to the pre- sence of vapour, the original bull being considered as unity.
		0		0		0	
0	1.0012	26	1.0042	51	1'0125	76	1.0299
1	1,0012	27	1.0049	52	1.0129	77	1.0309
2	1,0019	28	1.0021	53	1.0134	78	1.0319
3	1.0014	29	1.0023	54	1.0139	79	1,0330
4	1.0018	30	1.0026	55	1.0144		1.0341
5	1.0018	31	1.0028	56	1.0120	81	1'0352
	1.0010	32	1.0000	57	1.0122	82	1.0364
7 8	1'0020	33	1.0063	58	1,0191	83	1'0376
8	1'0020	34	1.0062	59	1.0164	84	1.0389
9	1.0071	35	1.0068	60	1.0123	85	1'0402
10	1.0023	36	1,0041	61	1'0179	86	1.0414
II	1'0024	37	1'0074	62	1.0182	87	1'0427
12	1'0025	38	1'0077	63	1.0105	88	1.0441
13	1.0076	39	1.0080	64	1.0199	89	1'0455
14	1'0027	40	1.0083	65	1.0206	90	1.0470
15	1.0029	41	1.0086	66	1'0213	91	1'0485
16	1.0030	42	1.0089	67	1'0220	92	1.0500
17	1,0031	43	1'0093	68	1.0228	93	1.0516
17	1.0033	44	1.0006	69	1.0236	94	1.0532
19	1.0034	45	1,0100	70	1'0244	95	1'0549
20	1.0036	46	1.0104	71	1'0253	96	1.0566
21	1.0038	47	1.0108	72	1.0262	97	1.0584
22	1'0039	48	1.0115	73	1'0271	98	1.0602
23	1.0041	49	1,0119	74	1.0380	99	1'0620
24	1.0043	50	1'0120	75	1'0289	100	1,0630
25	1.0042		100	100			-

Weight of Vapour in a Cubic Foot of Air.

Vapours, so long as they remain in an aëriform state, expand by the increase of temperature as permanently elastic fluids, and suffer changes of volume proportional to the changes of pressure. Air, as before stated, expands

1/491·13, or ·0020361 for every increase of 1° of heat; it therefore expands 0·3665 of its bulk from 32° to 212°, and its expansion is uniform between

these points.

Therefore, if the weight of a cubic foot of vapour, under the pressure of 30 inches of mercury, and at the temperature of 212° , be called W, and the weight expressed in the same denomination, of an equal volume of vapour, at the temperature t, and under the same pressure of 30 inches, be called W', and if E_t be the elasticity of vapour at the temperature t, then (the expansion of dry air from 32° to 212° being 0.3665, or 0.0020361 for each degree of temperature),

 $W' = \frac{1.3665 \times W \times E_t}{30\{1 + .0020361 \times (t^{\circ} - 32^{\circ})\}}.$

A cubic foot of vapour at 212°, and under a pressure of 30 inches, weighs 258.448 grains. Therefore, substituting this value of a cubic foot of vapour at 212°, and under a pressure of 30 inches, the above formula becomes

$$\mathbf{W}' \!=\! \frac{1 \!\cdot\! 3665 \times 258 \!\cdot\! 448 \times \mathbf{E}_t}{30\{1 + \!\cdot\! 0020361 \times (t^\circ \!-\! 32^\circ)\}}.$$

And from this formula the next Table has been formed.

Table VI.—Showing the Weight in Grains of a Cubic Foot of Vapour, under the pressure of 30 inches of Mercury, for every degree of temperature, from 0° to 100°.

Temp. Fahr.	Weight in grains of a Cubic Foot of Vapour.	Temp. Fahr.	Weight in grains of a Cubic Foot of Vapour.	Temp. Fahr.	Weight in grains of a Cubic Foot of Vapour.	Temp. Fahr.	Weight in grains of a Cubic Foot o Vapour.
	grs.	26	grs. 1.68		grs.	7 ⁶	grs.
0	0.22			51	4'24		9.69
I	0.24	27	1.75	52	4'39	77	. 9.99
2	0.20		1.82	53	4.55	78	10.31
3	0.62	29	1.89	54	4.71	79 80	10.64
4	0.65	30	1.97	55	4.87	81	10.08
5	0.68	31	2.02	56	5'04	82	11.32
	0.41	32	2.13	57	5.51	83	11.67
7 8	0'74	33	2.51	58	5:39	84	12.03
	0.77	34	2,30	59	5.28	85	12.40
9	0.80	35	2.39	60	5.77	86	12.78
10	0.84	36	2.48	62	5:97	87	13.17
11	0.88	37	2.22		6.17	88	13.27
12	0.05	38	2.66	63	6.38		13.08
13	0.96	39	2.76	64	6.29	89	14.41
14	1.00	40	2.86	65	(0.000)	90	14.85
15	1.04	41	2.97	66	7.04	91	15'29
	1.09	42	3.08	67	7.27	92	15.74
17	1.14	43	3.50		7.51	93	16.60
18	1.19	44	3.35	69	7:76	94	
19	1'24	45	3'44	70	8.01	95	17.18
20	1.30	46	3.26	71	8:27	96	18.50
21	1.36	47	3.69	72	8.54	97	18.73
22	1.42	48	3.82	73	8.82	. 98	19.28
23	1.48	49	3.96	74	9,10	99	19.84
24	1.24	50	4.10	75	9.39	100	1904
25	1.01				10000		

From the numbers in this Table, it appears that the capacity of air for moisture doubles for a rise from 0° to 16°; from 16° to 33°; from 33° to 52°; from 52° to 73°; and from 73° to 96°; so that if the quantities of water held in solution be taken in a geometrical progression, the temperatures increase in a quicker ratio than the terms of an arithmetical progression.

When the readings of the dry- and wet-bulb thermometers are alike, the weight of a cubic foot of vapour is at once taken from the numbers in Table VI. In all other cases as the quantity of vapour at the temperature of the dewpoint expands in the same ratio as air, the weight of a cubic foot of vapour is

calculated from the following formula :-

Weight of a cubic foot of vapour.

Volume of temperature of dew-point × weight of a cubic foot of vapour at temperature of dew-point Volume at temperature of air.

Sum of the Weights of a Cubic Foot of Air and a Cubic Foot of Vapour.

Table VII.—Showing the Weight of a Cubic Foot of Dry Air added to the Weight of a Cubic Foot of Vapour, at all temperatures between 0° and 100°, under a pressure of 30 inches of Mercury.

Temp. Fahr.	Sum of the weights of a Cubic Foot of Dry Air and of a Cubic Foot of Vapour.	Temp. Fahr.	Sum of the weights of aCubic Foot of Dry Air and of a Cubic Foot of Vapour.	Temp. Fahr.	Sum of the weights of a Cubic Foot of Dry Air and of a Cubic Foot of Vapour.	Temp. Fahr.	Sum of the weights of aCubic Foot of Dry Air and of a Cubic Foot of Vapour.
0	grs.	26	grs.	0	grs.	0	grs.
0	606.92		575'55	-51	549'98	76	529'94
1	605.62	27	574'44	52	549'06	77	529'27
2	604.33	28	573'33	53	548-16	78	528.62
3	603.02	29	572'23	54	547.26	79	527.99
4	601.78	30	571'14	55	546.37	80	527.37
5	600.21	31	570'06	56	545'49	81	526.75
	599'25	32	568.98	57 58	544.62	82	526.15
7 8	598.00	33	567.91	58	543'75	83	525.26
8	596.75	34	566.86	59	542'90	84	524'99
9	595.21	35	565.81	60	542'05	85	524.43
10	594.58	36	564.76	61	541.22	86	523.88
11	593.06	37	563.72	62	540'39	87	523'34
12	591.84	38	562.68	63	539.58	88	522.82
13	590.63	39	561.65	64	538.77	89	522.32
14	589.43	40	560.63	65	537.98	90	521.84
15	588.23	41	559.63	66	537'20	91	521'36
16	587'04	42	558.63	67	536.42	92	520.89
17	585.86	43	557.64	68	535.65	93	520.44
18	584.68	44	556.66	69	534.90	94	520'01
19	583.21	45	555.68	70	534.16	95	219.29
20	582.35	46	554'71	71	533'43	96	210.18
21	581.50	47	553'75	72	532.71	97	518.80
22	580.06	48	552.79	73	532'00	98	518.43
23	578.92	49	551.85	74	531.30	99	518.00
24	577.78	50	550'92	75	530.61	100	Control of the Contro
25	576.66				33	-	517.77

The next Table is computed from the following formula:-

Weight of a cubic foot of saturated air.

Weight of a cubic foot of air and a cubic foot of vapour (Table VII.)

Increase of volume of a cubic foot of dry air in consequence of its saturation with moisture (Table V.).

Weight of a Cubic foot of Saturated Air.

Table VIII.—Showing the Weight in Grains of a Cubic Foot of Air saturated with moisture, at all temperatures between 0° and 100°, under the pressure of 30 inches of Mercury.

Temp. Fahr.	Weight of a Cubic Foot of Air saturated with Vapour.	Temp. Fahr.	Weight of a Cubic Foot of Air saturated with Vapour.	Temp. Fahr.	Weight of a Cubic Foot of Air saturated with Vapour.	Temp. Fahr.	Weight of a Cubic Foot of Air saturated with Vapour.
6	grs.		grs.		grs.	0	grs.
0	606.03	26	572.85	51	543'21	76	514'55
1	604.69	27	571'63	52	542'06	77	513'40
2	603.37	28	570'42	53	540.89	78	512'26
3	602.05	29	569'20	54	539'75	79	511.13
4	600'72	30	567'99	55	538.60	80	509'97
5	599'40	31	566.79	56	537'45	81	508.81
	598.11	32	565.28	57	536.30	82	507.67
7 8	596.80	33	564.38	58	535'16	83	506.21
8	595'51	34	563.18	59	534'00	84	505.36
. 9	594'24	35	561.99	60	532.84	85	504.19
10	592'94	36	560'79	61	531.69	86	503.05
II	591.64	37	559'59	62	530'55	87	501.90
12	590'35	38	558.42	63	529'42	88	500.74
13	589.08	39	557'22	64	528'27	89	499'57
14	587.82	40	556.03	65	527.14	90	498.43
15	586.55	41	554.87	66	526'01	91	497'25
16	585.30	42	553.69	67	524.86	92	496.07
17	584.03	43	552'52	68	523'71	93	494'90
18	582.76	44	551.36	69	522'55	94	493'74
19	581.21	45	550'19	70	521'41	95	492.56
20	580'26	46	549'01	71 ·		96	491.39
21	579'03	47	547.85	72	519'12	97	490'19
22	577'78	48	546.69	7-3	517'98	98	489'01
23	576.56	49	545'53	74	516.82	99	487.83
24	575'32	50	544'36	75	515.69	100	486.65
25	574.08	100 100		1000000		Sales Con	The second second

When the readings of the two thermometers are alike, the weight of a cubic foot of air, under a pressure of 30 inches of mercury, will be found opposite to

the temperature in the above Table.

In all other cases it is necessary to multiply the degree of humidity into the excess of the weight of a cubic foot of dry air (Table IV.) above that of a cubic foot of saturated air (Table VIII.), and to take the product from the weight of a cubic foot of dry air: the result will be under a pressure of 30 inches of mercury. The numbers in the General Tables have been calculated for a pressure of 29 inches.

Degree of Humidity.

In calculating the numbers in the Tables saturation has been assumed as 100, and air without moisture as zero. The numbers are found by dividing the quantity of vapour corresponding to the temperature of the dew-point, by the quantity which would have been present had the air been saturated.

ON THE MANNER OF USING THE TABLES.

To find the Temperature of the Dew-Point.

Case I.—If the readings of both the dry- and wet-bulb thermometers be whole degrees, the dew-point will be found opposite to the reading of the wet-bulb.

Case II.—If the reading of the dry-bulb be affected with parts of a degree, in the fourth column, opposite to the reading of the wet-bulb, will be found the amount of the decrease in the temperature of the dew-point, corresponding to an increase of reading of 1° in the dry-bulb. A proportional part of this, for the parts of a degree, is to be taken from the dew-point opposite to the

reading of the wet-bulb.

Case III.—If the readings of the dry- and wet-bulb be both affected with parts of a degree, then the decrease due to the excess above the whole degree in the dry will be found as in Case II.; and the increase due to the excess of reading of the wet-bulb above the whole degree will be found by taking the difference between two consecutive dew-points, which will give the difference for an increase of one degree in the wet-bulb: a proportional part of this being taken and applied will give the reading required.

Example.—Suppose the readings of the dry- and wet-bulb be 51°.6 and

46°.4.

In Table, 51° dry, on page 10,—

The dew-point opposite to 46° wet is $$ 40.8 The dew-point opposite to 47° wet is $$ 42.8
Difference, or the increase in dew-point for an increase of 1° in wet
Temperature of the dew-point corresponding to 51° dry and 46° 4 wet is
In the fourth column the decrease of dew-point for an increase of 1° in the dry is 0.9, the proportional part for 0.6 is
The temperature of dew-point corresponding to 51°·6 dry and 46°·4 wet is

In like manner the elastic force of vapour, the weight of vapour in a cubic foot of air; the additional weight required to saturate a cubic foot of air, and the degree of humidity may be found.

To find the weight of a cubic foot of air the reading of the barometer is

required in addition.

Example.—Required the weight of a cubic foot of air when the reading of the dry-bulb is 51°.6, wet 46°.4, and barometer 29.72 inches.

In column 13, opposite 46° wet is	525·9
dry is 1 gr.; the proportional part for 0°6 is	-0.6
Carried over	525.3

In column 14, the increa						r a	n i	ncr	eas	e ii	n tl	ne	525·3
Opposite '7 (in the Table Opposite '02 (in the little	un	der	. 18	3.1	in	las	t co	olu	mn)	is			12.7
page)													0.4
The weight required is .		1								80			538.4

When the reading of the barometer exceeds 30 inches, the numbers in column 13 are to be increased by the quantity in column 14 for one inch, and still further increased by the quantities in the little Tables in the last column, corresponding to the excess of reading above 30 inches.

When the reading is less than 29 inches, the difference from 29 inches is to be taken, and the quantities from the small Tables, corresponding to the difference, are to be taken and applied subtractively to the number in co-

lumn 13.

In all cases throughout the Tables the sign - denotes decrease, and the sign + increase.

General Remarks.

In addition to its value to the meteorologist, there are many cases in ordinary life in which this instrument may be used to advantage; the simple inspection of the two thermometers will often afford a better criterion of the weather, and of the probability of rain, than the barometer itself: regard, however, must be had to the time of the day and the time of the year when the observation is made.

In summer, when the diurnal range of temperature is great, if in the morning the difference between the air-temperature and the dew-point temperature be small, and the rise of temperature during the day considerable, it is probable that the difference will increase; and if the temperature of the dew-point at the same time decrease, it is an indication of very fine weather. If, on the contrary, the temperature of both should increase with the day in nearly equal proportion, rain will almost certainly follow as the temperature of the air falls with the declining sun.

In winter, when the diurnal range of temperature is small, the indication of the weather is shown by the increase or decrease in the temperature of the dew-point, rather than by the difference between the temperatures of the air and of the dew-point. In showery weather the indications vary rapidly, and a person making observations at short intervals may predict the approach of a storm, particularly if he take simultaneous observations with the baro-

meter.

Use of the Instrument in the Sick Chamber.

The importance of this instrument in the requirements of a sick chamber are scarcely to be over-rated, and will be at once obvious to all who know that the comfort of the patient is dependent not so much on the temperature, as on the hygrometric condition of the air. In cold frosty weather the air of apartments is frequently too dry, in which case the difference between the readings of the two thermometers will be great, and this condition will be manifest to the patient by the degree of inconvenience experienced attributable to this cause. If the air be moist, the difference between the

readings will be less, in proportion to the degree of moisture; and if the air be saturated, the readings will be alike. It would be well for the medical profession to enforce, as far as lies in its power, the use of this simple and effectual instrument, which in case of sickness gives indications so important to the comfort of the patient. If the air in the apartment be too dry, that is to say, if the difference between the readings of the thermometers is very considerable, it will be necessary to expose water in some shallow vessel of some extent of surface, so that the evaporation from it, mixing with the air, will cause a greater degree of humidity. This process may be considerably accelerated by heating the water, when the evaporation will proceed more rapidly.

If, on the contrary, the air be too moist, or should be required to be remarkably dry, all water must either be removed or covered over; and the required degree of dryness obtained either by raising the temperature, or by placing in the room sulphuric acid, or any other medium which has the property of rapidly absorbing watery vapour. By these simple means an artificial locality may be produced, and invalids whose circumstances or avocations prevent them from seeking a climate suited to their peculiar constitution may to a great extent, by the assistance of this instrument, obviate the

necessity of so doing.

The instrument in use should be placed in a part of the room away from the immediate influence of the fire, and not exposed to open doors or currents of air; in ordinarily constructed rooms, the best place is in a recess on the same

side of the room as the fire.

A difference of from 6 to 8 degrees between the readings of the two thermometers will generally be found to give a pleasant degree of humidity.

Use of the Instrument in Hothouses, Greenhouses, and in Conservatories.

In regulating the hygrometrical state of the air in conservatories, &c., it may be made to render essential service, the temperature of the air being regulated by the dry-bulb, and the degree of humidity by the lower reading of the wet-bulb.

It is well known that in greenhouses plants become shrivelled or otherwise injured before there is any suspicion of an alteration in the humidity of the air; and when suspected, a quantity of water, without any guide as to the amount required, is thrown upon the plants and walls; and occasionally at other times, when our senses indicate a dry atmosphere, water is spread in the same indefinite manner. Our sensations, with regard to heat and humidity, are very fallacious guides: every one must have felt in summer the heat at times to be almost insupportable, without any apparent reason as shown by the reading of the thermometer; this happens when the air is nearly calm and moist; and should the air become in motion, under the same hygrometric conditions we feel cool, and experience a relief; should these hygrometric conditions change, with the same temperature, and the air become dryer, evaporation of moisture from the skin takes place with activity, and we feel a marked sensation of cold; so that with the same temperature, and enjoying an equal state of health, we experience according to our own sensations various vicissitudes of temperature; in fact, our senses cannot guide us with regard to heat and humidity. A dry- and wet-bulb thermometer properly used, and its indications attended to, may be made the means of preserving many valuable plants which might otherwise perish in an ill-regulated atmosphere.

To make the instrument properly available for this purpose, a knowledge is required of the climatic conditions of the countries in which the plants naturally have their growth. The temperature of the hothouse may then be regu-

lated by the dry, and the degree of humidity by the wet bulb. For example, suppose the temperature of the climate be 70°, and its mean state of humidity about 60 or 70 per cent. of the quantity of aqueous vapour which the air would contain if saturated. It is necessary then that the reading of the dry thermometer should be maintained at 70°, and the reading of the wet between 60° and 64°. These last numbers are found by looking in the Table at div. 70° of the dry bulb, and under degree of humidity for 60 or 70, which give corresponding readings between 61° and 65°. The introduction of a large surface of water with a moveable cover to regulate at pleasure the extent of evaporating surface, is a certain means of obtaining and afterwards continuing the required degree of humidity: should it be found desirable to throw water on the walls, the attendant will find in the instrument a certain guide as to the degree of humidity in the air occasioned by the performance of this operation, which he will regulate accordingly.

Value of the Instrument in places where Stoves are used.

The use of stoves is general, but their effects are often injurious to health, and frequently subject the occupant of rooms so heated to much pain and inconvenience; this arises in a great measure from the excessive dryness of the air of such rooms, causing moisture from the skin to evaporate too rapidly.

Blackheath, April 1866.

of 7	ding Ther- neter.	Temperature of the Dew-point.	Difference for an in- crease of 1° in Dry.	Elastic force of Vapour.	Difference for an in- crease of 10 in Dry.	Vapour in a Cubic Foot of Air.	Difference for an in- crease of 1° in Dry.	Vap. reqd. to sat. a Cubic Foot of Air.	Difference for an in- crease of 1° in Dry.	Degree of Humi- dity. (Satn. = 100.)	Difference for an in- crease of 10 in Dry.	Weight of a Cubic Foot of Air. Bar. reading 29 inches.	Diff. for an increase of 10 in Dry	Difference for one inch in Barometer and proportional parts.
10	9.8 9.6 9.4 9.2 9.0	10°0 8°2 6°5 4°7 3°0 1°2	-7.8 7.8 7.7 7.7 7.7 -7.7	in. 0'068 0'063 0'058 0'054 0'050 0'046	in'020 '018 '016 '015 '014'012	gr. 0'8 0'8 0'7 0'7 0'6 0'6	gr. -0'2 0'2 0'2 0'2 0'2 -0'2	gr. 0'0 0'1 0'2 0'2 0'2	gr. +0'2 0'2 0'2 0'2 0'2 +0'2	100 92 85 78 72 67	-33 29 26 23 20 -18	grs. 573'1'2'2'2'2'3 573'3	+10.8	19'8 in. grs. '1 2'0 '2 4'0 '3 5'9 '4 7'9 '5 9'9
111	11'0 10'8 10'6 10'4 10'2 10'0 9'8	11'0 9 2 7'5 5'7 4'0 2'2 0'5	-7.8 7.8 7.7 7.7 7.7 7.7 -7.7	0'071 0'065 0'060 0'056 0'052 0'048	-*021 *018 *016 *014 *012 *010 -*008	0°9 0°8 0°7 0°7 0°6 0°6	-0'2 0'2 0'2 0'2 0'2 0'2 -0'2	0°0 0°1 0°2 0°3 0°3	+0'2 0'2 0'2 0'2 0'2 0'2 +0'2	100 92 85 78 72 67 62	-34 30 27 24 22 20 -18	571'9 572'0 '0 '1 '1 572'1	+19.7	.2 9 17.8 .6 11.9 .7 13.9 .8 15.8 .9 17.8
12	12'0 11'8 11'6 11'4 11'2 11'0 10'8	12.0 10.2 8.5 6.7 5.0 3.2 1.5	-7.8 7.8 7.8 7.7 7.7 7.7 7.7 -7.7	0°074 0°068 0°063 0°058 0°054 0°050 0°047	-*022 *020 *018 *016 *014 *012 -*010	0.9 0.8 0.7 0.7 0.6 0.6	0°2 0°2 0°2 0°2 0°2 0°2 0°2	0°0 0°1 0°2 0°3 0°3	+0.3 0.3 0.3 0.3 0.3 0.3	100 92 85 78 72 66 61	-34 31 28 26 24 22 -20	570'7 '7 '8 '8 '8 '8	+19.7	19'7 '1 2'0 '2 4'0 '3 5'9
13	13.0 12.8 12.6 12.4 12.2 11.6 11.8	13.0 11.3 9.5 7.7 6.0 4.2 2.5 0.7	-7.8 7.8 7.8 7.7 7.7 7.7 7.7 7.7 7.7	0°078 0°072 0°066 0°061 0°056 0°052 0°048	-'023 '021 '019 '017 '015 '013 '011 -'009	1°0 0°9 0°8 0°7 0°7 0°6 0°6	-0'3 0'2 0'2 0'2 0'2 0'2 -0'2	0°0 0°1 0°2 0°3 0°3 0°4	+0.3 0.3 0.3 0.3 0.3 0.3 0.3	100 92 85 78 72 66 61 57	-34 31 28 25 23 21 19 -18	569°5 °6 °6 °6 °7 7 569°7	+19.6	'4 7'9 '5 9'9 '6 11'9 '7 13'9 '8 15'8 '9 17'8
14	14'0 13'8 13'6 13'4 13'2 13'0 12'8 12'6	14°0 12°2 10°5 8°7 7°0 5°2 3°5 1°7	-7·8 7·8 7·8 7·7 7·7 7·7 7·7 -7·7	0'082 0'075 0'069 0'064 0'059 0'055 0'051 0'048	- '025 '022 '020 '018 '016 '014 '012 - '010	1°0 0°9 0°8 0°7 0°7 0°6 0°6	-0'3 0'3 0'3 0'2 0'2 0'2 0'2 -0'2	0'0 0'1 0'1 0'3 0'3 0'4	+0.3 0.3 0.3 0.3 0.3 0.3 0.3	100 92 85 78 72 66 61 57	30 28 26 24 22 20	568·2 '3 '3 '3 '4 '4 '4 568·5	+10.6	19.6 1 2.0 2 3.9 3 5.9 4 7.8
15	15.0 14.8 14.6 14.4 14.2 14.0 13.8 13.6	15°0 13°3 11°5 97 8°0 6°2 4°5 2°7 1°0	-7.7 7.7 7.7 7.7 7.7 7.6 7.6 7.6 7.6	0°086 0°079 0°073 0°062 0°057 0°053 0°049 0°046	- '026 '024 '022 '020 '018 '016 '014 '012 - '010	1°1 1°0 0°9 0°8 0°7 0°7 0°6 0°6	-0.3 0.3 0.3 0.3 0.3 0.3 0.2 0.2 0.2	0°1 0°2 0°3 0°4 0°4 0°5	+0.3 0.3 0.3 0.3 0.3 0.3	92 85 78 72 67 62	-33 30 27 25 24 22 19 17	'1 '1 '2 '2 '2	+19.6	5 9.8 6 11.8 7 13.7 8 15.6 9 117.6
16	16°0 15'8 15'6 15'4 15'2 15'0 14'8 14'6 14'4	16.0 14.3 12.5 10.8 9.0 7.3 5.6 3.8 2.1	-7.6 7.6 7.6 7.6 7.5 7.5 7.5 7.5 7.5 7.5 7.4	0.090 0.083 0.046 0.040 0.065 0.060 0.051 0.047 0.044	-'027 '025 '022 '020 '018 '016 '014 '012 '010 -'008	1'1 1'0 0'9 0'9 0'7 0'7 0'6 0'6 0'6	-0'3 0'3 0'3 0'3 0'3 0'2 0'2 0'2 0'2 -0'2	0°1 0°2 0°3 0°4 0°4 0°5 0°5	+0.3 0.3 0.3 0.3 0.3 0.3 0.3 0.3	100 92 85 79 73 67 62 58 53	-32 29 27	565.8	+19.2	'01 0'2 '02 0'4 '03 0'6 '04 0'8 '05 1'0 '06' 1'2 '07 1'4 '08 1'6 '09 1'8

of T	ding her- ieter.	Temperature of the Dew-Point.	Difference for an in- erease of 1º in Dry.	Elastic force of Vapour.	Difference for an in- crease of 1° in Dry.	Vapour in a Cubic Foot of Air.	Difference for an in- crease of 10 in Dry.	Vap. read. to sat. a Cubic Foot of Air.	Difference for an in- crease of 1º in Dry.	Degree of Humidity. (Satur.=100.)	Difference for an in- crease of 1° in Dry.	Weight of a Cubic Foot of Air. Bar. reading 29 inches.	Diff. for an inc case of 10 in Dry	Difference for one inch in Barometer and proportional parts.
17	17'0 16'8 16'6 16'4 16'2 16'0 15'8 15'6 15'4 15'4	17.0 15.3 13.6 11.8 10.1 8.4 6.7 4.9 3.2 1.5	-7.5 7.5 7.5 7.4 7.4 7.3 7.3 7.3 7.3	in. 0'094 0'087 0'080 0'074 0'068 0'058 0'054 0'050 0'047	in'028 '026 '023 '021 '019 '017 '015 '013 '011'009	gr. 1'1 1'0 1'0 0'9 0'8 0'7 0'6 0'6 0'6	gr0'3 0'3 0'3 0'3 0'2 0'2 0'2 0'2 0'2 -0'2	gr. 0'0 0'1 0'2 0'3 0'4 0'5 0'5	gr. +0'4 0'4 0'4 0'3 0'3 0'3 0'3 0'2 0'2 +0'2	93 86 80 74 68 63 58 53	- 32 30 28 26 24 22 20 18 16 - 14	grs. 564.5 -6 -6 -7 -7 -7 -8 -8 -8 -8 -9 564.9	+10.2 - 1.1 drs.	19'5 in. gr. 1 2'0 '2 3'9 '3 5'9 '4 7'8 '5 9'8 '6 11'7 '7 13'7 '8 15'6
18	18.0 17.8 17.6 17.4 17.2 17.0 16.8 16.6 16.4 16.2 16.0	18.0 16.3 14.6 12.9 11.2 9.5 7.8 6.1 4.4 2.7 1.0	-7.3 7.3 7.3 7.3 7.2 7.2 7.1 7.1 7.0 -6.9	0'098 0'091 0'084 0'077 0'071 0'066 0'061 0'057 0'053 0'049	-*028 *026 *024 *022 *020 *018 *016 *014 *012 *010 -*008	1'2 1'1 1'0 0'9 0'8 0'7 0'7 0'6 0'6	-0'3 0'3 0'3 0'3 0'3 0'2 0'2 0'2 0'2 0'2 -0'2	0'0 0'1 0'2 0'3 0'4 0'5 0'6 0'6 0'6	+0°4 0°4 0°4 0°4 0°3 0°3 0°3 0°2 0°2 +0°2	93 86 80 74 68 63 58 54 50 46	-32 30 28 26 23 21 19 17 15 13 -11	563'4 '5 '5 '6 '6 '6 '7 '7 563'8	+19.4	19'4
19	19.0 18.8 18.6 18.4 18.2 18.0 17.8 17.6 17.4 17.2 17.0 16.8	19°0 17°3 15°7 14°0 12°3 10°7 9°0 7°3 5°6 4°0 2°3 0°7	-7°1 7°1 7°0 7°0 6°9 6°8 6°8 6°7 6°7 -6°7	0'103 0'095 0'088 0'081 0'075 0'070 0'065 0'066 0'055 0'051 0'048	'030 '027 '025 '022 '020 '019 '017 '015 '013 '011 '009 '008	1'3 1'2 1'1 1'0 0'9 0'9 0'8 0'7 0'6 0'6	-0'3 0'3 0'3 0'3 0'3 0'3 0'3 0'2 0'2 0'2 0'2 -0'2	0'0 0'1 0'2 0'3 0'4 0'5 0'6 0'6 0'7 0'7	+0.4 0.4 0.3 0.3 0.3 0.3 0.2 0.2 0.2 0.2 0.2 0.2	93 86 80 74 68 63 58 54 50 47	-32 29 27 25 22 20 18 17 16 14 13 -11	562°1 °2 °3 °3 °4 °4 °5 °5 °5 °5 °5	+19.4	'2 3'9 '3 5'8 '4 7'8 '5 9'7 '6 11'6 '7 13'6 '8 15'5 '9 17'5
20	20'0 19'8 19'6 19'4 19'2 19'0 18'8 18'6 18'4 18'2 18'0 17'8	20°0 18°4 16°7 15°1 13°5 11°9 10°2 8°6 7°0 5°4 3°7 2°1	-6.9 6.8 6.7 6.7 6.7 6.6 6.5 6.5 6.4 6.4 6.4 -6.3	0°108 0°100 0°093 0°086 0°079 0°073 0°068 0°063 0°055 0°055 0°051 0°048	- '030 '028 '026 '024 '021 '019 '017 '015 '014 '013 '012 '011 - '010	1'3 1'2 1'1 1'0 0'9 0'8 0'8 0'7 0'7 0'6 0'6	-0.3 0.3 0.3 0.3 0.3 0.2 0.2 0.2 0.2 0.2 0.2 0.2	0'0 0'1 0'2 0'3 0'3 0'4 0'5 0'6 0'6 0'7 0'7	+0'4 0'4 0'4 0'4 0'3 0'3 0'3 0'3 0'3 0'2 +0'2	93 86 80 74 68 63 59 55 51 48 45 42	28 26 24 22 20 18 16 15 14 13	561.0 10 11 12 12 13 13 14 14 14 14 15 16 17 17 18 18 18 18 18 18 18 18 18 18	+19.3	19'3 '1 1'9 '2 3'9 '3 5'8 '4 7'7 '5 9'7 '6 11'6 '7 13'5 '8 15'4 '9 17'4
21	21'0 20'8 20'6 20'4 20'2 20'0 19'8 19'6 19'4 19'2 19'0 18'8 18'6 18'4	21°0 19°4 17°9 16°3 14°7 13°1 11°5 10°0 8°4 6°8 5°2 3°7 2°1 0°5	-6.6 6.5 6.5 6.4 6.3 6.2 6.2 6.1 6.1 6.0 6.0 -5.9	0'113 0'105 0'097 0'090 0'084 0'078 0'072 0'067 0'062 0'058 0'054 0'051 0'048	- '030 '028 '025 '023 '021 '019 '017 '016 '014 '013 '012 '011 '010 - '010	1'4 1'3 1'2 1'1 1'0 0'9 0'8 0'8 0'7 0'7 0'6 0'6	-0.3 0.3 0.3 0.3 0.3 0.3 0.3 0.2 0.2 0.2 0.2 0.2 0.2 0.2 0.2	0'0 0'1 0'2 0'3 0'4 0'4 0'5 0'6 0'6 0'7 0'7 0'8 0'8	+0'4 0'4 0'3 0'3 0'3 0'3 0'2 0'2 0'2 0'2 0'2 0'2 0'2 +0'2	100 93 87 81 75 70 65 60 56 52 49 46 43 40	27 25 23 21 20 18 16 15 14 13 12	559'7 '8 '8 '9 559'9 560'0 '0 '1 '1 '1 '2 '2 '2 '560'2	+19.3	*01 0'2 '02 0'4 '03 0'6 '04 0'8 '05 1'0 '06 1'2 '07 1'4 '08 1'6 '09 1'8

of	sading Ther- ometer.	Temperature of the Dew-Point.	Difference for an in- crease of 1° in Dry.	Elastic force of Vapour.	Difference for an in- crease of 1° in Dry.	Vapour in a Cubic Foot of Air.	Difference for an in- crease of 1° in Dry.	Vap. read. to sat. a Cubic Foot of Air.	Difference for an in- crease of 1° in Dry.	Degree of Humi- dity. (Satn.=100.)	Difference for an in-	Weight of a Cubic Foot of Air. Bar. reading 29 inches.	Diff. for an increase of 10 in Bar.	Difference for one inch in Barometer and proportional parts.
22		22'0 20'5 19'0 17'4 15'9 14'4 12'9 11'4 9'8 8'3 6'8 5'3 3'8 2'2	6.2 6.0 6.0 6.0 5.9 5.8 5.7	in. 0'118 0'110 0'102 0'095 0'089 0'083 0'077 0'072 0'067 0'063 0'055 0'051 0'048	in'030 '027 '025 '023 '022 '020 '018 '017 '015 '014 '013 '012 '010'010	gr. 1'4 1'3 1'2 1'1 1'0 0'9 0'8 0'8 0'7 0'7 0'6 0'6	gr0'3 0'3 0'3 0'3 0'3 0'2 0'2 0'2 0'2 0'2 0'2 0'2 0'2 -0'2	gr. o'o o'1 o'2 o'3 o'4 o'5 o'6 o'6 o'7 o'7 o'7 o'8 o'8	gr. +0'4 0'4 0'4 0'3 0'3 0'3 0'3 0'3 0'3 0'2 0'2 0'2 +0'2	100 94 88 82 76 71 66 62 58 54 50 47 44 41 38	- 28 26 24 23 21 19 18 16 15 15 14 13 12 - 11	·5.6 ·6 ·6 ·7 ·7 ·8 ·8	- 1'1 +19'3	19'3 in. grs. '1 1'9 '2 3'9 '3 5'8 '4 7'7 '5 9'7 '6 11'6 '7 13'5 '8 15'4 '9 17'4
23	23°0 22°8 22°4 22°4 22°2 21°8 21°6 21°4 21°2 20°6 20°4 20°2	23°0 21'5 20'1 18'6 17'2 15'7 14'3 12'8 11'4 9'9 8'4 7'0 5'5 4'1 2'6	-5'9 5'8 5'8 5'7 5'6 5'5 5'4 5'4 5'3 5'2 5'2 5'1 5'0 -5'0	0'123 0'115 0'108 0'101 0'094 0'088 0'082 0'077 0'072 0'067 0'063 0'055 0'055 0'055	-*029 '027 '026 '024 '022 '020 '018 '017 '016 '014 '013 '012 '011 '010 -'010	1'5 1'4 1'3 1'2 1'1 1'1 1'0 0'9 0'8 0'8 0'7 0'7 0'6 0'6	-0'3 0'3 0'3 0'3 0'3 0'2 0'2 0'2 0'2 0'2 0'2 -0'2	0°0 0°1 0°2 0°3 0°4 0°4 0°5 0°6 0°6 0°7 0°7 0°8 0°8 0°8	+0'4 0'4 0'3 0'3 0'3 0'3 0'2 0'2 0'2 0'2 0'2 0'2 +0'2	94 88 82 77 72 67 63 59 55 52 48 45 42 39	-27 25 23 22 20 19 17 16 15 14 13 12 11 10 - 9	557'4 '4 '5 '5 '6 '6 '6 '7 '7 '7 '7 '8 '8 '8 '8 '9	+19'2	19'2 'I 1'9 '2 3'8 '3 5'8 '4 7'7 '5 9'6 '6 11'5 '7 13'4 '8 15'4 '9 17'3
24	24'0 23'8 23'6 23'4 23'2 23'0 22'8 22'6 22'4 22'2 21'8 21'6 21'4 21'2 21'0	24'0 22'6 21'2 19'8 18'5 17'1 15'7 14'3 12'9 11'5 10'2 8'8 7'4 6'0 4'6 3'2	-5.5 5.4 5.3 5.2 5.2 5.2 5.2 5.2 5.2 5.4 6.4 6.4 6.5 4.5 4.5 4.5	0°129 0°121 0°114 0°107 0°100 0°064 0°082 0°077 0°072 0°068 0°064 0°066 0°056 0°053	'029 '027 '025 '023 '021 '020 '019 '017 '015 '013 '012 '011 '010 '009 '009	1'5 1'5 1'4 1'3 1'2 1'1 1'0 0'9 0'9 0'8 0'7 0'7 0'6 0'6	-0.3 0.3 0.3 0.3 0.3 0.3 0.3 0.3	0°0 0°1 0°2 0°3 0°3 0°4 0°4 0°5 0°6 0°6 0°7 0°7 0°8 0°8 0°9	+0'4 0'4 0'3 0'3 0'3 0'3 0'3 0'3 0'2 0'2 0'2 0'2 0'2 +0'2	94 88 83 78 73 69 65 61 57 53 50 47 44 42 39	24 23 21 20 18 17 15 14 13 12 12 11 10	556·1 ·2 ·2 ·3 ·3 ·4 ·4 ·5 ·5 ·6 ·6 ·6 ·6 ·6 ·6	+19.2	19°1 11 1°9 2 3°8 3 5°7 4 7°6 5 9°6 6 11°5 7 13°4 7 13°4 8 15°3 9 17°2
一 一 日本本本の	25'0 24'8 24'6 24'4 24'2 24'0 23'8 23'6 23'4 23'2 23'0 22'8 22'6 22'4	25°0 23°7 22°4 21°1 19°8 18°5 17°2 15°9 14°6 13°3 11°9 10°6 9°3 8°0 6°7	-5'1 5'0 4'9 4'8 4'7 4'6 4'5 4'4 4'3 4'2 4'1 4'0 3'9 -3'8	0'135 0'127 0'120 0'113 0'106 0'100 0'094 0'089 0'084 0'079 0'065 0'065 0'065	'028 '026 '024 '022 '020 '019 '018 '017 '016 '014 '013 '012 '011 '010 '010	1.6 1.5 1.4 1.4 1.3 1.2 1.1 1.0 0.9 0.8 0.9 0.9	-0'3 0'3 0'3 0'3 0'3 0'2 0'2 0'2 0'2 0'2 0'2 0'2 0'2 -0'2	0°1 0°2 0°3 0°4 0°5 0°5 0°6 0°6 0°7 0°8 0°8	+0.4 0.4 0.4 0.4 0.3 0.3 0.3 0.3 0.3 0.3 0.3 0.2 0.2 +0.2	100 - 94 89 84 79 74 70 66 62 59 55 52 49 46 43 -	22 21 20 18 17 16 14 13 12 11 10 9 8	555.0 11 12 12 13 13 14 14 14 14 15 15 15 15 15 15 15 15 15 15 15 15 15		01 0'2 02 0'4 03 0'6 04 0'8 05 1'0 06 1'2 07 1'3 08 1'5

of 7	ding Ther- neter.	Temperature of the Dew-Point,	Difference for an in- crease of 1° in Dry.	Elastic force of Vapour.	Difference for an in- crease of 1° in Dry.	Vapour in a Cubic Foot of Air.	Difference for an increase of 10 in Dry.	Vap. reqd. to sat. a Cubic Foot of Air.	Difference for an in- crease of 1° in Dry.	Degree of Humidity. (Satn.=100.)	Difference for an in- crease of 1° in Dry.	Weight of a Cubic Foot of Air. Bar. reading 29 inches.	Diff. for an increase of 10 in Dry	Difference for one inch in Barometer and proportional parts.
Dry.	Wet. 26°0 25'8 25'6 25'4 25'2 25'0 24'8 24'6 24'4 24 2 24'0 23'8 23 6 23'4 23'2	26.0 24.8 23.6 22.3 21.1 19.9 18.7 17.5 16.3 15.1 13.8 12.6 11.4 10.2 9.0	-4.6 4.5 4.4 4.3 4.2 4.1 4.0 4.0 3.9 3.8 3.7 3.6 3.5 3.5 -3.4	in. 0'141 0'134 0'127 0'120 0'113 0'107 0'101 0'096 0'091 0'086 0'081 0'076 0'072 0'068 0'065	in '027 '025 '023 '021 '019 '018 '017 '016 '015 '014 '013 '012 '011 '010 - '009	gr. 1'77 1'6 1'5 1'4 1'3 1'2 1'1 1'0 1'0 0'9 0'9 0'8 0'8	6.1 6.1 6.1 6.1 6.1 6.1 6.1 6.1	gr. 0.0 0.1 0.2 0.3 0.4 0.5 0.6 0.6 0.7 0.7 0.8 0.8 0.9 0.9	gr. +0.3 0.3 0.3 0.3 0.3 0.3 0.3 0.3 0.1 0.1 0.1 0.1 0.1 0.1	100 95 90 85 80 76 72 68 64 61 58 55 52 49	-211 200 188 177 166 15 144 131 121 111 100 100 9	gra. 553'7 '8 '9 553'9 554'0 '0 '0 '1 '1 '2 '2 '2 '2 '3 554'3	+10.1 +10.1	19'1 in. grs. '1 1'9 '2 3'8 '3 5'7 '4 7'6 '5 9'6 '6 11'5 '7 13'4 '8 15'3 '9 17'2
28	27.0 26.8 26.6 26.4 26.2 26.0 25.8 25.6 25.4 25.2 25.0 24.8 24.6 24.4 24.2 28.0 27.8 27.6 27.4 27.2 27.0 26.8 26.6 26.6 26.6 26.6 27.4 27.2 27.0 26.8 27.6 27.4 27.2 27.0 26.8 27.6 27.4 27.2 27.6 27.6 27.6 27.6 27.6 27.6 27.6	27.0 25.9 24.8 23.6 22.5 21.4 20.3 19.2 18.0 16.9 15.8 14.7 13.5 12.4 11.3 28.0 27.0 26.0 24.9 23.9 22.9 21.9 20.8 19.8	-4.1 4.0 3.9 3.8 3.7 3.6 3.5 3.4 3.3 3.2 3.1 3.0 2.9 2.8 -2.7 -3.6 3.5 3.4 3.3 3.2 3.1 3.0 2.9 2.8 -2.7 -3.6 3.5 3.7 3.6 3.7 3.7 3.7 3.7 3.7 3.7 3.7 3.7	0'147 0'140 0'133 0'126 0'120 0'114 0'109 0'104 0'099 0'094 0'089 0'084 0'080 0'076 0'072 0'153 0'146 0'140 0'134 0'128 0'122 0'117 0'112 0'107 0'102 0'097 0'093 0'089 0'085	- '025 '023 '021 '010 '018 '017 '016 '015 '014 '013 '012 '011 '010 - '023 '021 '020 '019 '018 '016 '015 '014 '013 '012 '011 '010 - '010 '019 '018 '016 '015 '014 '013 '012 '011 '010 010 '009	1'7 1'7 1'6 1'5 1'4 1'4 1'3 1'2 1'1 1'0 1'0 0'9 0'9 1'8 1'7 1'6 1'5 1'5 1'4 1'3 1'3 1'2 1'1 1'1 1'0	-0'3 0'3 0'2 0'2 0'2 0'2 0'2 0'1 0'1 0'1 0'1 -0'3 0'3 0'3 0'2 0'2 0'2 0'2 0'2 0'1 0'1 0'1 0'1 0'1 0'1 0'1 0'1 0'1 0'1	0.0 0.1 0.1 0.2 0.3 0.4 0.5 0.6 0.6 0.7 0.7 0.8 0.8 0.9 0.1 0.2 0.3 0.3 0.4 0.5 0.6 0.7 0.7 0.7 0.7 0.7 0.7 0.7 0.7 0.7 0.7	+0.3 0.3 0.3 0.3 0.3 0.3 0.3 0.3 0.3 0.3	100 95 91 87 83 79 75 71 68 64 61 58 55 52 49 100 95 91 87 84 80 76 73 70 64 61 61 63 64 61 64 65 67 64 67 67 67 67 67 67 67 67 67 67	18 17 16 15 14 13 12 11 10 9 8 7 - 7 - 18 16 15 14 14 13 12 11 10 10 10 10 10 11 11 11 11 11 11 11	56.66.66.77.78.88.89.99.99	+10.0 - 1.1 +10.1	19'0 '1 1'9 '2 3'8 '3 5'7 '4 7'6 '5 9'5 '6 11'4 '7 13'3 '8 15'2 '9 17'1
29	25'2 29'0 28'8 28'6 28'4 28'2 28'0 27'8 27'6 27'4 27'2 27'0 26'8 26'6 26'4 26'2	29.0 28.1 27.2 26.2 25.3 24.4 23.4 22.5 21.6 20.7 19.7 18.8 17.9 17.0 16.0	-2.4 -3.1 3.0 2.9 2.8 2.7 2.6 2.5 2.4 2.3 2.2 2.1 2.0 1.9 -1.8	0'081 0'160 0'154 0'148 0'142 0'136 0'125 0'120 0'115 0'106 0'102 0'098 0'094	- '009 - '020 '019 '018 '017 '016 '014 '013 '012 '011 '010 '009 '008 '008 - '007	1.0 1.8 1.8 1.7 1.6 1.6 1.5 1.4 1.3 1.3 1.2 1.2 1.1	-0.1 -0.1 -0.1 -0.1 -0.1 -0.1 -0.1 -0.1	0.8 0.0 0.1 0.1 0.2 0.3 0.3 0.4 0.5 0.6 0.6 0.7 0.7 0.8	+0.5 +0.3 0.3 0.3 0.3 0.3 0.3 0.3 0.3	53 100 96 93 89 86 82 79 76 73 70 67 64 61 58 56	- 17 16 15 14 14 13 12 12 11 10 9	550.2	+10.0	'01 0'2 '02 0'4 '03 0'6 '04 0'8 '05 1'0 '06 1'2 '07 1'3 '08 1'5 '09 1'7

of mo	eading Ther- ometer.	Temperature of the Dew-Point,	Difference for an in- crease of 1° in Dry.	Elastic force of Vapour.	Difference for an in- crease of 1° in Dry.	Vapour in a Cubic Foot of Air.	Difference for an in- crease of 1° in Dry.	Vap. read. to sat. a Cubic Foot of Air.	Difference for an in- crease of 1° in Dry.	Degree of Humi- dity. (Satn.=100).	Difference for an in-	Weight of a cubic Foot of Air. Bar. reading 20 inches.	Diff. for an increase of 10 in Dry	Difference for one inch in Barometer and proportional parts.
o 30	30°0 29°8 29°6 29°4 29°2 29°0 28°8	30°0 29°2 28°3 27°5 26°7 25°9 25°0	2.7 2.6 2.5 2.4 2.4 2.3 2.2	n. 0°167 0°161 0°155 0°150 0°145 0°140	in'019 '018 '017 '016 '015 '014 '013	gr. 2'0 1'9 1'8 1'7 1'7	gr. -0'2 0'2 0'2 0'2 0'2 0'2 0'2	g . 0'0 0'1 0'2 0'2 0'3 0'3	0.3 0.3 0.3 0.3 0.3 0.3 0.3	100 96 93 90 86 83 80	- 15 14 14 13 12 11	grs. 549'1' '1' '2' '2' '2' '2' '3'	+ 18.0 - 1.1 grs.	18'9 in. grs. '1 1'9 '2 3'8 '3 5'7 '4 7'6 '5 9'5
	28.6 28.4 28.2 28.0 27.8 27.6 27.4 27.2	24'2 23'4 22'5 21'7 20'9 20'0 19'2 18'4	2'1 2'0 1'9 1'8 1'7 1'7 1'6	0'130 0'125 0'120 0'116 0'112 0'104 0'104	'012 '011 '010 '009 '008 '008 '008 -'007	1'5 1'4 1'4 1'3 1'3 1'2	-0.1 0.1 0.1 0.1 0.1 0.1 0.1 0.1	0.2 0.2 0.6 0.4 0.7 0.7 0.8 0.8	0'2 0'2 0'2 0'2 0'2 0'2 0'2	77 75 72 69 67 64 62 60		'3 '4 '4 '5 '5 '5	1 Black	'6 11'3 '7 13'2 '8 15'1 '9 17'0
31	30.8 30.6 30.4 30.2 30.0 29.8 29.6 29.4	31°0 30°3 29°5 28°8 28°0 27°3 26°6 25°8 25°1	2.1 2.1 2.0 1.0 1.0 1.8 1.7	0'174 0'168 0'163 0'158 0'153 0'148 0'143 0'135	'017 '015 '014 '013 '012 '011 '010 '010 '010	2.1 2.0 1.9 1.8 1.7 1.6 1.6	-0'2 0'2 0'2 0'2 0'1 0'1 0'1	0°0 0°1 0°2 0°2 0°3 0°4 0°4 0°5 0°5	+0.2 0.2 0.3 0.3 0.1 0.1 0.1	96 93 90 87 85 82 79	-13 12 12 11 10 9 9 8 8	547'9 547'9 548'0 '0 '1 '1 '1 '2 '2	+18.9	
32	29°2 29°0 28°8 28°6 28°4 28°2 32°0 31°8	24'3 23'6 22'9 22'1 20'6 32'0 31'3	1.6 1.5 1.5 1.4 1.3 -1.2	0'131 0'127 0'123 0'119 0'115 0'111	*010 *009 *008 *007 -*007	1.2 1.4 1.4 1.4 1.4 1.4 1.4	0.1 0.1 0.1 0.1 0.1 0.1	0.6	+0.1 +0.1 0.1 0.1 0.1	74 72 70 68 66 64 100 97	7 7 6 6 6 - 5 - 11	*2 *3 *3 *3 548*3 546*7	- 1,1	
	31.6 31.4 31.2 31.0 30.8 30.6 30.4 30.4	30.7 30.0 29.3 28.7 28.0 27.4 26.7 26.7	1'9 1'8 1'7 1'7 1'6 1'6 1'5	0'172 0'167 0'162 0'157 0'153 0'149 0'145	'013 '012 '011 '010 '010 '010 '009 '008	2.0 2.0 1.9 1.8 1.8 1.8	0'2 0'2 0'2 0'1 0'1 0'1 0'1	0'1 0'1 0'2 0'3 0'3 0'4	0.3 0.3 0.3 0.3 0.3	94 92 89 87 84 82 79	10 9 8 8 7	320	+18.9	
33	30°0 29°8 29°6 29°4 29°2 33°0 32°8	25'4 24'7 24'0 23'4 22'7 33'0 32'4	1'3 1'3 1'2 1'1 -1'1		'008 '008 '008 '007 -'007	1.6 1.6 1.5 1.4 2.2 2.2	0'1 0'1 0'1 -0'1 -0'2		0°2 0°2 0°2 +0°3 0°3	75 73 71 69 67	6 6 5 5 5	.0 .0 .1 .1 547'1	- 1.1	
	32.6 32.4 32.2 32.0 31.8 31.6 31.4 31.4	31.8 31.2 30.6 30.0 29.4 28.8 28.2 27.6	1'7 1'6 1'6 1'5 1'5 1'4 1'4	0.179 0.122 0.123 0.123 0.123 0.123 0.123	,000 ,010 ,010 ,011 ,011 ,011 ,011	2'1 2'0 2'0 1'9 1'8 1'8	0.1 0.1 0.1 0.1 0.1 0.5	0°1 0°1 0°2 0°2 0°3 0°3 0°4	0'3 0'3 0'2 0'2 0'2 0'2	95 93 91 89 86 84 82 80	10 9 9 9 8 8		695	'01 0'2 '02 0'4 '03 0'6
	31.0 30.8 30.6 30.4 30.4	27.0 26.4 25.8 25.2 24.6	1'3 1'3 1'3 1'2 -1'2	0'147 0'143 0'136 0'136 0'136	*009 *009 *009 *008 *008	1.4 1.6 1.6 1.6	-0.1 0.1 0.1 0.1 0.1	0.2	0°2 0°2 0°2 0°2 +0°2	78 76 74 72 71	7 7 7 6	.9 .9 545.9 546.0 546.0		'04 0'8 '05 1'0 '06 1'1 '07 1'3 '08 1'5 '09 1'7

		1 =	1 0 -	1 5	è.	10	l è ·	a .	4.7	1.0	4 .	10	1 8	
1	Aller	Temperature of the Dew-Point.	Difference for an in crease of 1° in Dry	io o	Difference for an in- crease of 1° in Dry.	Cubic	an in Dry.	Vap. reqd. to sat	Difference for an in crease of 1° in Dry.	Degree of Humi- dity. (Satn.=100,	Difference for an in crease of 1° in Dry.	Weight of a Cubic Foot of Air. Bar. reading 29 inches.	for an increas 1º in Dry in. in Bar.	Difference for one inch in Barometer and proportional parts.
of T	ding her-	it it	o for	force	o for	in a Air.	Difference for crease of 1° in	. to	for	H H	for	Weight of a Cubi Foot of Air. Bar reading 29 inches	for an inc. 1° in Dry in. in Bar.	for
mon	neter.	Poin	e of		to of	of A	ence of j	For	Difference for	Sat (Sat	of 1	of Ai	o in	Difference inch in Ba and prop
-	-	emp car	Differe	Elastic Vapour,	iffer	Vapour Foot of	iffer	ap.	iffer	egre ty.	iffer	eigh adin	# 1-	Differe inch ir and parts.
Dry.	Wet.	83	0.9	H>	0.5	DA	99	>0	A P	D.B	AB	SE 5	of Di	Diff.
0	24'0	34'0	- 1.6	in. 0'196	in.	gr. 2'3	gr. -0'2	gr.	+0.3	100	- 10	grs.	grs.	
34	34.0	33.2	1.6	0,105	'012	5.3	0'2	0.0	0.3	98	-10	544'4	- 1.1	18.8
	33.6	32.9	1.2	0.188	*012	2'2	0.3	0,1	0.3	96	10	*4	+18.8	in. grs.
	33'4	31.8	1.2	0.180	'012	2'2 2'I	0'2	0.1	0.3	93	9	. 5		'1 1'9
	33'0	31'2	1.4	0.146	'012	2.1	0,1	0'2	0'2	89	9	· 5 · 5 · 6		3 5.6
100	32.8	30.1	1'4	0.12	110,	2'0	0,1	0,3	0.5	87 85	9 9 8 8	.6		5 94
	32.4	29.6	1.3	0'164	.010	1,9	0.1	0.4	0'2	83	8	.6	1000	.2 13.3
100	32.5	29'0	1.3	0.160	.009	1.0	0,1	0.4	0.5	81	8 7 7 7 7 6	.6	100	.8 12.0
	31.8	28.5	1,3	0.129	,008	1.8	0.1	0.2	0'2	79	7	.7	Ban B	.0 16.9
	31.6	27'4	1.2	0.148	,008	1.8	0,1	0.2	0.5	76	7	.7		
	31.4	26.8	-1.1	0'145	-,008	1.7	0,0	0.6	+0.1	74	- 6	544.8		
	31.5		-	0'142	000	1.7	00	30	101	73		244 0	- 1.1	1
35	350	35.0	-1.2	0'204	011	2'4	-0'2	0,0	+0.3	98	-10	543'3	+18.7	
1	34.8	34'5	1.2	0,100	110,	2.3	0'2	0.1	0.3	98	9	.3 .4	+18.7	
	34'4	33'4	1.2	0'192	,010	2'2	0'2	0'2	0.3	94	98	.4		
	34'2	32'9	1.4	0'188	.010	5.1	0.7	0.3	0.3	92	8	.4		
	33.8	31.9	1.4	0,180	.000	2'1	0,1	0.3	0'2	88	8	*4 *5 *5 *5 *6		2.36
	33.6	31'4	1.4	0'176	.008	2'1	0.1	0.3	0'2	86	8	.5	100	1000
	33'4	30.3	1'4	0.12	*007	2'0	0,1	0.4	0'2	82	7 7 7 7 6	.5		
	33'0	29.8	1.3	0'164	.006	1.9	0.1	0.2	0'2	80	7		100	
	32.8	28.8	1.3	0.160	.006	1,0	0.1	0.2	0'2	79	7	.6	NO.	-0
	32.4	28.5	1,5	0.124	.006	1.8	0.1	0.6	0'2	75	.6	.6		18.7
	32'2	27.7	1.5	0,121	.006	1.8	0.0	06	0,1	74	- 6	.7	13 44	2 3.8
	32'0	27.2	-1.7	0.148	006	1.7	-0.0	07	+0.1	12	- 0	543'7	· march	.3 2.6
36	36	36.0	-1.4	0'212	-'012	2.2	-0.1	0,0	+0'2	100	- 9 8	542'1	- 1.1	'4 7'5 '5 9'4
	35 34	33.2	1.3	0.122	,010	2'2	0.1	0.3	0.5	91 82		'2	+18.7	.6 11.5
	33	28.5	1'2	0,128	.000	1.8	0,1	0.4	0'2	74 66	7 6 5 5 4	·4 ·5 ·6		.4 12.0
	32	26.0	1.1	0'142	*007	1.7	0,1	0.8	0.5	59	5	.6		.9 16.8
	31	23.2	1.0	0,113	.006	1.2	0.1	1.5	0'2	53	4	.7		
	29	18.5	0.0	0,101	'005	1.5	0.1	1.3	0'2	47	4	542.9		
	28	16.0	-0.8	0,000	004	1.1	-0.1	1.4	+0.5	42	- 3	543.0		2
37	37 36	34.6	1.3	0'220	-,015	2.9	-0.1	0.0	+0.5	91	- 9 8	240.9	- 1.1	1
	35	32'2	1.3	0.185	.000	2.1	0.1	0.2	0'2	83	7	'2	+18.4	1
	34	29.7	1'2	0.162	*008	1.4	0,1	0.0	0.5	75 68	6	·3	2	
1	33	27'3	1,1	0.149	.006	1.6	0.1	1.0	0'2	61		.5	No B	
	31	22.2	1.0	0'120	1005	1'4	0.1	1.5	0'2	55	5		100	3 100
	30	17.6	0.8	0.104	*004	1.1	0,0	1.2	0.1	49	4 3	.7		12
	28	15.5	-0.8	0.086	003	1.0	-0.0	1.6	+0.1	39	- 2	541.8	3 1916	A STATE OF
38	38	38.0	-1.3	0'228	-,010	2.7	-o.1	0.0	+0.5	100	- 8	539.8	- 1.1	
	37 36	35'6	1,3	0.100	.009	2.4	0, I 0, I	0.2	0'2	91 83	7 6	5400	+18.6	'01 0'2
	35	30.0	1'2	0'173	'009	2'0	0,1	0.4	0'2	75 68	6	.2		'02 0'4
1	34	28.6	1.2	0'157	.008	1.8	0.1	0.0	0'2	68	5	.3	4-1-4	·03 0·6
1	33	26 2	1.1 1.1	0'142	1007	1.2	0.1	1.0	0'2	56	5 4	·4 ·5	9 3 4	-05 0.9
1-1	31	21.2	1'0	0.112	'005	1.3	0.0	1'4	0.1	50	4		373	.09 1.1
1 100	30	16.8	1.0	0,103	1004	1.7	0.0	1.2	0,1	45	- 3 - 3	.7	100	.08 1.2
199	28	14.4	-0.9	0.083	003	1,0	-0.0	1.7	+0.1	37	- 3	540.8		.09 1.7
B	-													

of mo	Ther- meter.	Temperature of the Dew-Point.	Difference for an in- crease of 1° in Dry.	Elastic force of Vapour.	Difference for an in- crease of 1° in Dry.	Vapour in a Cubic Foot of Air.	Difference for an in- crease of 1° in Dry.	Vap. read. to sat. a Cubic Foot of Air.	Difference for an in- crease of 1° in Dry.	Degree of Humi- dity. (Satn.=100.)	Difference for an in- crease of 1° in Dry.	Weight of a Cubic Foot of Air. Bar.	Diff. for an increase of 1 in. in Bar.	Difference for one inch in Barometer and proportional parts.
39	9 39 38 37 36 35 34 33 32 31 30 29 28	39°0 36°7 34°4 32°0 29°7 27°4 25°1 22°8 20°4 18°1 15°8 13°5	-1'3 -1'3 -1'3 -1'3 -1'1 -1'1 -1'1 -1'0 -1'0 -1'0	in. 0'238 0'218 0'199 0'181 0'164 0'149 0'135 0'122 0'110 0'099 0'089	in*012 '011 '010 '009 '008 '007 '006 '005 '004 '003 '002 -*002	gr. 2.8 2.5 2.3 2.1 1.9 1.7 1.6 1.4 1.3 1.2	0.0 0.1 0.1 0.1 0.1 0.1 0.1 0.1 0.1	gr. o'o o'3 o'5 o'7 o'9 1'1 1'2 1'4 1'5 1'6	gr. +0'2 0'2 0'2 0'2 0'2 0'2 0'2 0'2 0'2 0'2	100 92 84 77 70 63 57 52 47 42 38	- 8 8 8 7 7 6 6 6 5 5 4 4	-8 538-9 539-0 -1 -2 -3 -4 -5 -6	+18.6	18·6 in. grs. '1 1'9 '2 3'7 '3 5'6 '4 7'4 '5 9'3 '6 11'2 '7 13'0 '8 14'9 '9 16'7
40	40 39 38 37 36 35 34 33 32 31 30 29	40°0 37°7 35°4 33°1 30°8 28°5 26°3 24°0 21°7 19°4 17°1 14°8	-1'2 1'2 1'1 1'1 1'1 1'1 1'1 1'0 1'0 1'0 0'9	0'247 0'226 0'227 0'189 0'172 0'156 0'142 0'117 0'166 0'096 0'087	'012 '011 '010 '009 '008 '007 '007 '007 '007 '007 '007 '007	0'9 2'9 2'6 2'4 2'2 2'0 1'8 1'6 1'5 1'4 1'2 1'1	0.1 0.1 0.1 0.1 0.1 0.1 0.1 0.1 0.1 0.1	1'9 0'0 0'3 0'5 0'7 0'9 1'1 1'3 1'4 1'5 1'7 1'8	+0'1 +0'2 0'2 0'2 0'2 0'2 0'2 0'2 0'2 0'2 0'2	34 100 92 84 76 69 63 57 51 46 42 38 34	- 3 8 8 7 6 5 5 4 4 3 3 3 3 3 3 3 2 2	*4 *5 *6 *7	+18.2	
41	28 1 41 40 39 38 37 36 35 34 33 32 31 30 29 28	12.5 41.0 38.7 36.5 34.2 32.0 29.7 27.4 25.2 22.9 20.7 18.4 16.1 13.9 11.6	-0'9 -1'2 1'1 1'1 1'0 1'0 1'0 1'0 0'9 0'9 0'9 0'9	0'078 0'257 0'235 0'215 0'197 0'180 0'164 0'149 0'135 0'122 0'110 0'099 0'089 0'080 0'072	-'006 -'012 '010 '008 '007 '006 '005 '005 '005 '005 '004 '003 '002 -'002	0'9 3'0 2'7 2'5 2'3 2'1 1'9 1'7 1'6 1'4 1'3 1'2 1'0 0'9	-0.0 0.0 0.0 0.1 0.1 0.1 0.1 0.1	2'0 0'0 0'3 0'5 0'7 0'9 1'1 1'3 1'4 1'6 1'7 1'8 2'0 2'1	+0'1 +0'2 0'2 0'2 0'2 0'2 0'2 0'2 0'2 0'2 0'1 0'1 +0'1	31 100 92 84 77 70 64 58 53 48 43 39 35 31 28	- 8 76 5 5 4 4 4 3 3 3 2 2	538.7 536.4 .5 .7 .8 536.9 537.0 .1 .2 .3 .4 .5 .5 .6 537.7	+18.2	18.5 1 1.9 2 3.7 3 5.6 4 7.4 5 9.3 6 11.1 7 13.0 8 14.8 9 16.7
42	42 41 40 39 38 37 36 35 34 33 32 31 30 29 28	42.0 39.8 37.5 35.3 33.1 30.9 28.6 26.4 24.2 21.9 19.7 17.5 15.2 13.0 10.8	-1'2 1'1 1'1 1'1 1'0 1'0 1'0 0'9 0'9 0'9 0'8 0'8 -0'8	0'267 0'245 0'225 0'207 0'190 0'174 0'159 0'144 0'130 0'117 0'106 0'096 0'087 0'078	-'012 '011 '010 '010 '009 '008 '007 '006 '005 '004 '004 '004 '004 -'004	3'1 2'8 2'6 2'4 2'2 2'0 1'8 1'7 1'5 1'4 1'2 1'1 1'0 0'9 0'8	-0.0 0.0 0.0 0.0 0.0 0.1 0.1 0.1 0.1 0.1	0°0 0°3 0°5 0°7 0°9 1°1 1°3 1°4 1°6 1°7 1°9 2°0 2°1 2°2 2°1	+0'2 0'2 0'2 0'2 0'2 0'2 0'2 0'2 0'2 0'2	100 92 85 78 72 66 60 54 49 44 40 36 33 30 27	- 8 8 7 7 6 6 5 5 4 4 3 2 2 2	535'2 '3 '5 '6 '7 '8 535'9 536'0 '1 '2 '3 '4 '5 536'6	+18.5	'01 0'2 '02 0'4
43	43 42 41 40 39 38	40.8 38.6 36.4 34.2	- 1'2 1'1 1'1 1'1 - 1'1	0°255 0°234 0°215 0°197	-'012 '010 '010 '009 -'009	3'2 2'9 2'7 2'5 2'3 2'1	-0.1 0.1 0.1 0.1 0.1 0.1	0.0	+0'2 0'2 0'2 0'2 0'2 +0'2	120 - 92 84 78 71	- 8 7 7 6	534'1		'03 0.6 'C4 0.7 '05 0.9 '06 1.1 '07 1.3 '08 1.5 '09 1.7

Read of T mom	her-	Temperature of the Dew-Point,	Difference for an in- crease of 1° in Dry.	Elastic force of Vapour.	Difference for an increase of 1° in Dry.	Vapour in a Cubic Foot of Air.	Difference for an in- crease of 10 in Dry.	Vap. reqd. to sat. a Cubic Foot of Air.	Difference for an in- crease of 10 in Dry.	Degree of Humidity. (Satn.=100.)	Difference for an in-	Weight of a Cubic Foot of Air. Bar. reading 29 inches.	Diff. for an increase of 10 in Dry 1 in. in Bar.	Difference for one inch in Baremeter and proportional parts.
43	38 37 36 35 34 33 32 31 30 29	32°0 29°8 27°6 25°4 23°2 21°0 18°8 16°6 14°4 12°2	-0.8 -0.8 -0.8 -0.9 -0.9 -0.9 -0.9	in. 0'181 0'166 0'152 0'138 0'125 0'113 0'102 0'092 0'083 0'074	in'009 '009 '009 '008 '007 '006 '005 '004 '003'003	gr. 2'1 1'9 1'7 1'6 1'4 1'3 1'2 1'1 1'0 0'9	-0,1 0,1 0,1 0,1 0,1 0,1 0,1 0,1	gr. 1'1 1'3 1'5 1'6 1'8 1'9 2'0 2'1 2'2 2'3	gr. +0'2 0'2 0'2 0'2 0'2 0'2 0'2 0'2 0'2 +0'2	65 59 54 49 45 41 37 34 31 28	- 6 5 5 4 4 4 3 3 3 3 3 3 3 3 3	grs. 534'8 534'9 535'0 '1 '2 '3 '3 '4 '5 535'5	grs 1·1	18'4 in. gr. '1 1'8 '2 3'7 '3 5'5 '4 7'4 '5 9'2 '6 11'0 '7 12'9 '8 14'7
44	44 43 42 41 40 39 38 37 36 35 34 33 32 31 30	44.0 41.8 39.6 37.5 35.3 33.1 30.9 28.7 26.6 24.4 22.2 20.0 17.8 15.7 13.5	-0.6 -0.6 -0.6 -0.6 -0.6 -0.6 -0.6 -0.6	0'288 0'265 0'244 0'224 0'205 0'188 0'172 0'157 0'143 0'130 0'118 0'107 0'097 0'088 0'080	'013 '012 '011 '010 '008 '007 '006 '005 '004 '003 '003 '003 '003	3'3 3'0 2'8 2'6 2'4 2'2 2'0 1'8 1'7 1'5 1'4 1'2 1'1 1'0 0'9	-0.0 0.0 0.0 0.0 0.1 0.1 0.1 0.1 0.1 0.1	0.0 0.3 0.5 0.7 0.9 1.2 1.3 1.5 1.6 1.8 1.9 2.1 2.2 2.3 2.4	+0'2 0'2 0'2 0'2 0'2 0'2 0'2 0'2 0'2 0'2	100 92 84 77 71 65 59 54 49 45 41 37 34 31 28	3 3 3 3 3	533.0 .1 .3 .4 .5 .6 .7 .8 533.9 534.0 .1 .2 .3 .3 .3 534.4	+18.4	9 16.6
45	45 44 43 42 41 40 39 38 37 36 35 34 33 32 31	45'0 42'8 40'7 38'5 36'4 34'2 32'0 29'9 27'7 25'6 23'4 21'2 19'1 16'9 14'8	-0.8 -0.9 0.9 0.9 0.9 0.9 0.0 1.0 1.0 1.0 1.0 1.0 1.0 1.0 1.0 1.0	0'299 0'275 0'253 0'253 0'214 0'197 0'181 0'166 0'152 0'139 0'127 0'115 0'104 0'094 0'085	'013 '011 '009 '008 '007 '007 '007 '007 '007 '007 '006 '005 '004'003	3'4 3'1 2'9 2'7 2'5 2'3 2'1 1'9 1'7 1'6 1'4 1'3 1'1 1'0	-0.0 0.0 0.0 0.0 0.0 0.0 0.1 0.1 0.1 0.1	0°0 0°3 0°5 0°7 0°9 1°1 1°3 1°5 1°7 1°8 2°0 2°1 2°2 2°3 2°4	+0'3 0'3 0'3 0'3 0'3 0'3 0'3 0'3 0'3 0'3	100 - 92 85 78 72 66 60 55 50 46 42 38 34 31 28	7 6 6 5 4 4 4 3 3 3 3	531'9 532'1 '2 '3 '5 '6 '7 '8 532'9 533'0 '1 '2 '2 '3 533'4	+18.3	18'3 '1 1'8 '2 3'7 '3 5'5 '4 7'3 '5 9'1 '6 11'0 '7 12'8 '8 14'6 '9 16'5
46	46 45 44 43 42 41 40 39 38 37 36 35 34 33 32	46.0 43.9 41.7 39.6 37.4 25.3 33.2 31.0 28.9 26.7 24.6 22.5 20.3 18.2 16.0	-0.8 -0.8 -0.9 -0.9 -0.9 -0.9 -0.9 -0.9 -0.9 -0.9	0'311 0'287 0'265 0'244 0'225 0'207 0'190 0'174 0'159 0'145 0'132 0'120 0'109 0'099	-'013 '012 '012 '011 '010 '009 '008 '007 '006 '005 '004 '004 -'003	3.6 3.3 3.1 2.8 2.6 2.4 2.2 2.0 1.8 1.7 1.5 1.4 1.3 1.1	-0'0 0'1 0'1 0'1 0'1 0'1 0'1 0'1	0.0 0.3 0.5 0.8 1.0 1.4 1.6 1.8 1.9 2.1 2.2 2.3 2.5 2.6	+0.3 0.3 0.3 0.5 0.5 0.5 0.5 0.5 0.5 0.5 0.5 0.7 0.7 0.7 0.7 0.7 0.7 0.7 0.7 0.7 0.7	93 86 79 73 67 61 56 51 47 43 39 35 32 29	7 7 6 6 5 5 4 4 4 3 3 3 3	530.7 530.9 531.0 2 3 3.4 55.6 8 531.9 532.0 0 11	+18.3	*01 0°2 *02 0°4 *03 0°6 *04 0°7
47	47 46 45 44 43	47°0 44'9 42'8 40'6 38'5	-1.0 1.0 1.1 1.1	0'323 0'298 0'275 0'253 0'233	-'014 '013 '012 '010 -'009	3.7 3.4 3.2 2.9 2.7	-0'1 0'2 0'1 -0'1	0.0	+0.3 0.3 0.3 0.5 +0.5	93 86 79 73	7 6 6	529.6 .7 529.9 530.0 530.1	+18.3	'04 0'7 '05 0'9 '06 1'1 '07 1'3 '08 1'5 '09 1'7

of T	ding Ther- neter.	Temperature of the Dew-point.	Difference for an in- crease of 1° in Dry.	Elastic force of Vapour.	Difference for an in- crease of 1° in Dry.	Vapour in a Cubic Foot of Air.	Difference for an in- crease of 1° in Dry.	Vap. reqd. to sat. a Cubic Foot of Air.	Difference for an in- crease of 1° in Dry.	Degree of Humi- dity. (Satn.=100.)	Difference for an in-	Weight of a Cubic Foot of Air. Bar. reading 29 inches.	Diff. for an increase of 10 in Dry	Difference for one inch in Barometer and proportional parts.
47	9 43 42 41 40 39 38 37 36 35 34 33	38.5 36.4 34.3 32.2 30.0 27.9 25.8 23.7 21.6 19.4	-1.0 1.0 1.0 1.0 0.9 0.9 0.9 0.9 0.9	in. 0'233 0'214 0'197 0'181 0'166 0'152 0'139 0'127 0'116 0'105 0'095	in '009 '008 '008 '008 '007 '006 '005 '005 '004 - '004	gr. 2'7 2'5 2'3 2'1 1'9 1'7 1'6 1'5 1'3 1'2	-0.0 0.0 0.0 0.1 0.1 0.1 0.1 0.1 0.1 0.1	gr. 1'0 1'2 1'4 1'6 1'8 2'0 2'1 2'2 2'4 2'5 2'6	gr. + 0'2 0'2 0'2 0'2 0'2 0'2 0'2 0'2 0'2 0'2	73 67 61 56 51 47 43 39 36 33 30	- 55 55 44 33 33 32 - 2	·4 ·5 ·6 ·7 ·8	+18.3	in. grs.
48	48 47 46 45 44 43 42 41 40 39 38 37 36 35 34	48.0 45.9 43.8 41.7 39.6 37.5 35.4 33.3 31.2 29.1 27.0 24.9 22.8 20.7 18.6	-0.8 -0.8 -0.8 -0.9 -0.9 -0.9 -0.9 -0.9 -0.9 -0.9 -0.9	0'335 0'335 0'285 0'263 0'224 0'206 0'189 0'173 0'146 0'134 0'122 0'111	'013 '011 '009 '008 '007 '006 '005 '004 '004 '004 '004 '004	3.8 3.5 3.3 3.0 2.8 2.6 2.4 2.2 2.0 1.8 1.7 1.5 1.4 1.3 1.2	-0.5 0.5 0.1 0.1 0.1 0.1 0.1 0.1 0.1 0.1 0.1 0.1	0.0 0.3 0.5 0.8 1.0 1.2 1.4 1.6 1.8 2.0 2.1 2.3 2.4 2.5 2.6	+0.3 0.3 0.3 0.3 0.3 0.3 0.3 0.3	100 93 86 79 73 67 62 57 52 48 44 40 36 33 30	- 77766655443333222-2	528.5 .7 528.8 530.0 .1 .2 .4 .5 .6 .7 .8 .9 530.9 531.0 531.1	<u>+ 18.5</u>	
49	49 48 47 46 45 44 43 42 41 40 39 38 37 36 35 34	49.0 46.9 44.8 42.8 40.7 38.6 36.5 34.4 32.4 30.3 28.2 26.1 24.0 22.0 19.9 17.8	-1,1 1,0 1,0 1,0 0,3 0,3 0,3 0,3 0,3 0,3 0,3 0,3 0,3 0	0°348 0°322 0°298 0°276 0°255 0°217 0°200 0°184 0°169 0°155 0°142 0°130 0°118 0°107 0°097	'014 '013 '012 '011 '010 '009 '009 '009 '008 '007 '006 '006 '006 '006 '006 '005 '004 '003	4.0 3.7 3.4 3.1 2.9 2.7 2.5 2.3 2.1 1.9 1.8 1.6 1.5 1.3 1.2 1.1	-0.5 0.1 0.1 0.1 0.1 0.1 0.1 0.1 0.1 0.1 0.1	0°0 0°3 0°6 0°9 1°1 1°3 1°5 1°7 1°9 2°1 2°2 2°4 2°5 2°7 2°8 2°9	+0.3 0.3 0.5 0.5 0.5 0.5 0.5 0.5 0.5 0.5 0.5 0.5	100 93 86 79 73 67 62 57 53 49 45 41 37 34 31 28	2		- 1°0 +18°2	
50	50 49 48 47 46 45 44 43 42 41 40 39 38 37 36 35 34	47'9 45'9 43'8 41'8 39'7 37'6 35'6 33'5 31'5 29'4 2/'3 25'3 23'2 21'2	-1'0 1'0 1'0 1'0 1'0 0'9 0'9 0'9 0'9 0'9 0'8 0'8 0'8 0'8 0'8	0'334 0'309 0'286 0'265 0'245 0'226 0'208 0'191 0'176 0'162 0'149 0'136 0'124 0'113 0'103	- '013 '012 '011 '010 '010 '009 '008 '007 '006 '006 '006 '006 '006 '006 '006	4'1 3'8 3'5 3'3 3'0 2'8 2'6 2'4 2'2 2'0 1'8 1'7 1'5 1'4 1'3 1'2 1'1	-0'2 0'2 0'1 0'1 0'1 0'1 0'1 0'1 0'1 0'1 0'1 0'1	0°0 0°3 0°6 0°8 1°1 1°3 1°5 1°7 1°9 2°1 2°3 2°4 2°6 2°7 2°8 2°9 3°0	+0'3 0'3 0'2 0'2 0'2 0'2 0'2 0'2 0'2 0'2 0'2 0'2	100 93 86 80 74 68 63 58 53 49 45 41 37 34 31 29 27	76655544333222222	*3		'01 0'2 '02 0'4 '03 0'6 '04 0'7 '05 0'9 '06 1'1 '07 1'3 '08 1'5 '09 1'7

Reading of Ther-		Temperature of the Dew-Point.	Difference for an in- crease of 1º in Dry.	force of	Difference for an in- crease of 1° in Dry.	n a Cubic	Difference for an in- crease of 1° in Dry.	Vap. reqd. to sat. a Cubic Foot of Air.	Difference for an in- crease of 1° in Dry.	(Satn.=100.)	Difference for an in-	Weight of a Cubic Foot of Air. Bar. reading 29 inches.	Diff. for an increase of 1° in Dry	Difference for one inch in Barometer and proportional purts.
mon	ueter.	pera	erene se of	Elastic Vapour.	erenc se of	Vapour in a (Foot of Air.	erenc se of	require Fo	erenc se of	Degree o dity. (Sat	re of 1	ght of A	for an im	in B pro
Dry.	Dry. Wet.		Tem Dew Diffe		Diff	Vap	Differe	Cub	Diffi	Deg	Diffe	Weight Foot of reading	of 1	Differ inch and parts
51	51 50 49 48 47 46 45 44 43 42 41 40 39 38 37 36 35 34	\$10 49.0 46.9 44.9 42.8 40.8 38.8 36.7 32.6 30.6 28.6 26.5 24.5 22.4 20.4 18.4 16.3	-10 10 09 09 09 09 09 09 08 08 08 08 08 08 08 07 07 07	in. 0'374 0'348 0'323 0'299 0'276 0'255 0'236 0'218 0'201 0'185 0'170 0'156 0'143 0'131 0'120 0'110 0'100 0'091	*004 *004 *004 *004 *003 -*003	gr. 4'2 3'9 3'6 3'4 3'1 2'9 2'7 2'5 2'3 2'1 1'9 1'8 1'6 1'5 1'4 1'2 1'1	-0.0 -0.0 -0.0 -0.0 -0.0 -0.0 -0.1 -0.1	gr. 0'0 0'3 0'6 0'8 1'1 1'3 1'5 1'7 1'9 2'1 2'3 2'4 2'6 2'7 2'8 3'0 3'1 3'2	gr. +0'3 0'3 0'3 0'3 0'3 0'3 0'3 0'3 0'3 0'3	93 86 80 74 68 63 58 54 50 46 42 38 35 32 29 27	- 7766 554443333322222 - 2	-6	grs 1'0	18'1 in. grs. '1 1'8 '2 3'6 '3 5'4 '4 7'2 '5 9'1 '6 10'9 '7 12'7 '8 14'5 '9 16'3
52	52 51 50 49 48 47 46 45 44 40 39 38 37 36 35	52.0 50.0 48.0 45.9 43.9 41.9 39.9 35.9 35.9 33.8 31.8 29.8 27.8 25.7 23.7 21.7 19.7	-1'0 1'0 0'9 0'9 0'9 0'9 0'9 0'8 0'8 0'8 0'8 0'7 0'7 0'7 -0'7	0'388 0'361 0'335 0'310 0'287 0'266 0'246 0'227 0'210 0'194 0'179 0'165 0'152 0'139 0'127 0'116 0'106	'014 '013 '012 '011 '010 '009 '008 '007 '007 '006 '005 '005 '005 '005 '005 '005 '005 '003 '003 '003	4'4 4'1 3'8 3'5 3'3 3'0 2'8 2'6 2'4 2'2 2'0 1'9 1'7 1'6 1'4 1'3 1'2 1'1	-0.5 0.5 0.0 0.1 0.1 0.1 0.1 0.1 0.1 0.1 0.1 0.1	0.0 0.3 0.6 0.9 1.1 1.4 1.6 1.8 2.0 2.2 2.4 2.5 2.7 2.8 3.0 3.1 3.2 3.3	+0.1 +0.1 -0.1 -0.1 -0.1 -0.1 -0.1 -0.1 -0.1 -	93 86 80 74 69 64 59 54 50 46 42 39 36 33 30 27 25	2	524°0 2 '4 '6 '7 524'9 5-50 '1 3 '4 5-50 7 7 7 8 525'9 526'0 526'0	+18.1	18.0 1 1.8 2 3.6 3 5.4 4 7.2 5 9.0 6 10.8 7 12.6 8 14.4 9,16.2
53	53 52 51 50 49 48 47 46 45 44 43 42 41 40 39 38 37 36 54 53 52	53°0 51°0 44°0 45°0 43°0 41°0 39°0 37°0 35°0 33°0 29°0 27°0 25°0 21°0 19°0 54°0 52°0 50°0	-1'0 1'0 0'9 0'9 0'9 0'8 0'8 0'8 0'8 0'7 0'7 0'7 0'7 0'7 0'7 0'7 0'7 0'7 0'7	0'403 0'374 0'347 0'322 0'299 0'277 0'257 0'257 0'238 0'220 0'203 0'188 0'174 0'160 0'147 0'135 0'124 0'113 0'103	-'015 '014 '013 '012 '011 '010 '009 '008 '007 '006 '006 '006 '005 '005 '005 '005 '005	4.5 4.2 3.9 3.6 3.4 3.1 2.9 2.7 2.5 2.3 2.1 2.0 1.8 1.7 1.5 1.4 1.3 1.2 4.7 4.4 4.1	-0'1 0'1 0'1 0'1 0'1 0'1 0'1 0'1 0'1 0'1	0°0 0°3 0°6 0°9 1°1 1°4 1°6 1°8 2°0 2°2 2°4 2°5 2°7 2°8 3°0 3°1 3°2 3°3	+0'3 0'3 0'3 0'3 0'3 0'3 0'3 0'3 0'3 0'3	93 86 80 74 69 64 59 55 51 47 43 39 36 33 30 28 26	4 4 4 3 3 3 3 2 2 2 2 7 7 6	'4 '6 '7 523'9 524'0 '1 '2 '3 '4 '5 '6 '7 '8 '9 524'9 521'8 522'0 '1	+18.0 - 1.0 +18.0	*01 0°2 *02 0°4 *03 0°5 *04 0°7 *05 0°9
	51 50 49 48	48.1 46.1 44.1 45.1	-0.8 0.0 0.0	0'334 0'310 0'288 '0267	- '007 '008 '008	3.0 3.2 3.2 3.8	-0,1 0,1 0,1 0,1	0'9 1'2 1'4 1'7	+0.3 0.3 0.3 0.3	80 74 69 64	6 5 - 4	.3 .5 .6 522.7		.09 1.9 .08 1.2 .08 1.2

Reading of Thermometer.		Temperature of the Dew-Point,	Difference for an in- crease of 1° in Dry.	Elastic force of Vapour.	Difference for an in- crease of 1° in Dry.	Vapour in a Cubic Foot of Air.	Difference for an in- crease of 10 in Dry.	Vap. reqd. to sat. a Cubic Foot of Air.	Difference for an in- crease of 1° in Dry.	Degree of Humi- dity. (Satn.=190.)	Difference for an in- crease of 1° in Dry.	Weight of a Cubic Foot of Air. Bar. reading 29 inches.	Diff. for an increase of 1° in Dry	Difference for one inch in Barometer and proportional parts.
Dry.	Wet.	Eq.	A 5			V.	Ab	CA		B A	9.5	P. P.	Di	D.9 8 8
54	48 47 46 45 44 43 42 41 40 39 38 37	42'1 40'1 38'2 36'2 34'2 30'2 28'3 26'3 24'3 22'3 20'3	-0.8 0.8 0.8 0.8 0.7 0.7 0.7 0.7 0.7 0.7 0.6 -0.6	in. 0'267 0'248 0'230 0'213 0'197 0'182 0'168 0'155 0'142 0'130 0'119 0'109	*007 *007 *006 *005 *004 *003 *003 -*003	gr. 3'0 2'8 2'6 2'4 2'2 2'1 1'9 1'7 1'6 1'5 1'3	-0.0 0.0 0.0 0.0 0.0 0.1 0.1 0.1 0.1 0.1	gr. 1'7 1'9 2'1 2'3 2'5 2'6 2'8 3'0 3'1 3'2 3'4	er. +0.3 0.3 0.3 0.3 0.3 0.3 0.3 0.3 0.3 0.3	64 59 55 51 47 43 40 37 34 31 28 26	- 4 4 3 3 3 3 3 2 2 2 2 2 2	522'9 523'0 '1 '2 '3 '4 '5 '6 '7 '8 523'8	+ 18.0	in. grs.
55	55 54 53 52 51 50 49 48 47 46 45 44 43 42 41 40 39 38	55.0 53.0 51.1 49.1 47.2 45.2 43.2 41.3 39.3 37.4 35.4 33.4 31.5 29.5 27.6 25.6 23.6 21.7	0'9 0'9 0'9 0'8 0'8 0'8 0'8 0'7 0'7 0'7 0'7 0'6 0'6 0'6	0'433 0'403 0'375 0'349 0'325 0'280 0'260 0'241 0'223 0'206 0'175 0'162 0'150 0'138 0'127 0'116	-014 012 010 009 008 007 006 006 006 006 006 006 006	4'9 4'5 4'2 3'9 3'7 3'4 3'1 2'9 2'7 2'5 2'3 2'1 2'0 1'8 1'7 1'6 1'4	-0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.1 0.1	0°0 0°4 0°7 1°0 1°2 1°5 1°8 2°0 2°2 2°4 2°6 2°8 2°9 3°1 3°2 3°3 3°5	+0.5 0.5 0.5 0.5 0.5 0.5 0.5 0.5	93 87 81 75 70 65 60 56 52 48 44 41 38 35 32 29 27	- 76 55 55 55 55 54 44 43 33 33 22 22 22 22	520.6 520.8 521.0 .2 .3 .5 .6 .8 521.9 522.0 .1 .2 .3 .4 .5 .6 .7 522.7	+18.0	17'9 '1 1'8 '2 3'6
56	56 55 54 53 52 51 50 49 48 47 46 45 44 43 42 41 40 39	56°0 54°1 52°1 50°2 48°2 46°3 44°4 42°4 40°5 38°5 36°6 34°7 32°7 30°8 28°8 26°9 25°0 23°0	-0'9 0'9 0'9 0'8 0'8 0'8 0'8 0'7 0'7 0'7 0'7 0'6 0'6 0'6 -0'6	0'449 0'419 0'391 0'365 0'340 0'317 0'295 0'274 0'254 0'235 0'171 0'158 0'146 0'135 0'124	- '015 '014 '014 '013 '013 '012 '011 '010 '008 '007 '005 '004 '004 '004	5°0 4'7 4'4 4'1 3'8 3'5 3'3 3'1 2'8 2'6 2'4 2'3 2'1 1'9 1'8 1'6 1'5 1'4	-0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0	0.0 0.3 0.6 0.9 1.2 1.5 1.7 1.9 2.2 2.4 2.6 2.7 2.9 3.1 3.2 3.4 3.5 3.6	+0.4 0.4 0.4 0.3 0.3 0.3 0.3 0.3 0.3 0.3 0.3 0.3 0.3	93 87 81 75 65 60 56 52 48 44 41 38 35 32 29	5 5 4 4 4 3 3 3 3 2 2 2 2 2	519.6 .8 519.9 520.1 .3 .5 .6 .7 520.9 521.0 .1 .2 .3 .4 .5 .6 .7 .7 .5 .6 .7 .7 .7 .7 .7 .7 .7 .7 .7 .7	- 1°0 +17°9	3 5.4 7.2 5 9.0 6 10.7 7 12.5 8 14.3 9 16.1
57	57 56 55 54 53 52 51 50 49 48 47 46 45	57°0 55°1 53°2 51°2 49°3 47°4 45°5 43°6 41°6 39°7 37°8 35°9 34°0	-0'9 0'9 0'8 0'8 0'8 0'8 0'7 0'7 0'7 -0'7	0'465 0'434 0'405 0'377 0'351 0'327 0'304 0'283 0'263 0'244 0'227 0'211 0'196	-'014 '013 '012 '011 '010 '009 '008 '008 '007 '006 '006 '006	5'2 4'8 4'5 4'2 3'9 3'7 3'4 3'2 3'0 2'7 2'5 2'4 2'2	-0'1 0'1 0'1 0'1 0'1 0'1 0'1 0'1 0'1 0'1	0.0 0.4 0.7 1.0 1.3 1.5 1.8 2.0 2.2 2.5 2.7 2.8 3.0	+0.4 0.3 0.3 0.3 0.3 0.3 0.3 0.3 0.3 0.3	93 87 81 75 70 65 61 57 53 49 45 42	6 5 5 4 4 4 4 3 3	.6	+17.9	'01 0'2 '02 0'4 '03 0'5 '04 0'7 '05 0'9 '06 1'1 '07 1'3 '08 1'4 '09 1'6

of mo	ading Ther- meter.	Temperature of the Dew-Point.	Difference for an in- crease of 1° in Dry.	Elastic force of Vapour.	Difference for an in- crease of 10 in Dry.	Vapour in a Cubic Foot of Air.	Difference for an in- crease of 10 in Dry.	Vap. reqd. to sat. a Cubic Foot of Air.	Difference for an in- crease of 1° in Dry.	Degree of Humi- dity. (Satn.=100).	Difference for an in-	Weight of a Cubic Foot of Air. Bar. reading 29 inches.	Diff. for an increase of 1° in Dry	P.8 P.
	Wet.	-	0	in.	in.	gr.	gr.	gr.	gr.	- A	9 5	-	of Di	Differ inch and parts.
57	45 44 43 42 41 40 39	34'0 32'0 30'1 28'2 26'3 24'4 22'4	0.6	0°196 0°181 0°167 0°154 0°142 0°131	- '006 '005 '004 '003 '003	2.2 2.0 1.9 1.4	0.0 0.0 0.0 0.0 0.0 0.0	3.0 3.2 3.3 3.5 3.6 3.7 3.8	+0'3 0'2 0'2 0'2 0'2 +0'3	39 36 33 30 28 26	- 2 2 2 2 2 2 2 2	·3 ·4 ·5 ·6	+17.0	in. grs. 'I 1'8 '2 3'6 '3 5'3 '4 7'1 '5 8'9
58	58 57 56 55 54 53 52 51 50 49 48 47 46 45 44 43 42 41	58.0 56.1 54.2 52.3 50.4 48.5 46.6 44.7 42.8 40.9 39.0 37.1 35.2 33.3 31.4 29.5 27.6 25.7 23.8	-0.9 0.9 0.9 0.9 0.8 0.8 0.8 0.8 0.8 0.8 0.8 0.8 0.8 0.7 0.7 0.7 0.7	0'482 0'451 0'451 0'393 0'367 0'342 0'318 0'296 0'275 0'256 0'238 0'221 0'205 0'176 0'163 0'163 0'151 0'139 0'128	-'015 '014 '013 '012 '010 '009 '008 '008 '008 '008 '008 '008 '00	5.4 5.0 4.7 4.4 4.1 3.8 3.6 3.3 3.1 2.9 2.7 2.5 2.3 2.1 2.0 1.8 1.7 1.6	-0'2 0'2 0'0 0'0 0'0 0'1 0'1 0'1 0'1 0'1 0'1 0'1	0°0 0°4 0°7 1°0 1°3 1°6 1°8 2°1 2°3 2°5 2°7 2°9 3°1 3°3 3°4 3°6 3°7 3°8 4°0	+0'4 0'4 0'4 0'3 0'3 0'3 0'3 0'3 0'3 0'3 0'3 0'3 0'3	93 87 81 76 71 66 61 57 53 49 46 43 40 37 34 31 28 26	3 3 3 2 2 2 2 2	517.4 517.8 518.0 11 3 55.6 6 7 518.9 519.0 12 2 3 3.4 15.6 6 6 519.7	+17:8	*6 10·7 '7 12·5 *8 14·2 '9 16·0
59	59 58 57 56 55 54 53 52 51 50 49 48 47 46 45 44 43 42 41 40	59'0 57'1 55'2 53'3 51'4 49'5 47'7 45'8 43'9 42'0 40'1 38'2 36'3 34'4 32'5 30'7 28'8 26'9 25'0 23'1	-0.8 0.8 0.8 0.8 0.8 0.8 0.8 0.8 0.8 0.7 0.7 0.7 0.7 0.7 0.7 0.7 0.7 0.7 0.7	0'500 0'467 0'436 0'407 0'380 0'354 0'330 0'287 0'267 0'248 0'230 0'213 0'197 0'182 0'169 0'157 0'145 0'124	-*015 *014 *013 *012 *011 *010 *009 *009 *009 *006 *005 *005 *004 *003 *003 *003 *003	5.6 5.2 4.9 4.6 4.3 4.0 3.7 3.5 3.2 3.0 2.8 2.6 2.4 2.2 2.1 1.9 1.8 1.6 1.5 1.4	-0.5 0.5 0.5 0.5 0.5 0.1 0.1 0.1 0.1 0.1 0.1 0.1 0.1 0.1 0.1	0'0 0'4 0'7 1'0 1'3 1'6 1'9 2'1 2'4 2'6 2'8 3'0 3'2 3'4 3'5 3'7 3'8 4'0 4'1 4'2	+0'4 0'4 0'4 0'4 0'3 0'3 0'3 0'3 0'3 0'3 0'3 0'3 0'3 0'3	100 94 88 82 76 71 66 61 57 53 49 46 43 40 37 34 31 29 27 25	6 6 5 5 5 4 4 4 4 3 3 3 3 3 2 2 2 2 2 2 2	516·2 ·4 516·8 517·0 ·2 ·3 ·5 ·6 ·8 517·9 518·0 ·1 ·2 ·3 ·4 ·5 ·6 ·6 ·8	- 1°0 +17°8	
60	59 58 57 56 55 54 53 52 51 50 49 48 47 46	60°0 58°1 56°2 54°4 52°5 50°6 48°7 46°8 45°0 43°1 41°2 39°3 37°4 35°6 33°7	-0.8 0.8 0.8 0.8 0.8 0.8 0.8 0.8	0.485 0.485 0.453 0.395 0.369 0.344 0.321 0.299 0.278 0.259 0.241 0.224 0.208	"015" "014" "013" "012" "011" "010" "010" "010" "009" "009" "009" "009" "008" "007" "006"	5.4 5.1 4.7 4.4 4.1 3.8 3.6 3.3 3.1 2.9 2.7 2.5 2.3	-0'2 0'2 0'1 0'1 0'1 0'1 0'1 0'1 0'1 0'1 -0'1 -0	0'4 0'7 1'1 1'4 1'7 2'0 2'2 2'5 2'7 2'9 3'1 3'3	+0.4 0.4 0.3 0.3 0.3 0.3 0.3 0.3 0.3 0.3 0.3 0.3	94 88 82 76 71 66 62 58 54 50 46 43 40 37	6 5 5 5 5 5 5 5 5 5 5 5 5 5 5 5 5 5 5 5	.3 -		*01 0*2 *02 0*4 *03 0*5 *04 0*7 *05 0*9 *06 1*1 *07 1*3 *08 1*4 *09 1*6

of T	Ther- neter.	Temperature of the Dew-Point.	Difference for an in- crease of 1° in Dry.	Elastic force of Vapour.	Difference for an increase of 1° in Dry.	Vapour in a Cubic Foot of Air.	Difference for an in- crease of 1° in Dry.	Vap. reqd. to sat. a Cubic Foot of Air.	Difference for an in- crease of 1° in Dry.	Degree of Humi- dity. (Satn.=100.)	Difference for an in- crease of 1° in Dry.	Weight of a Cubic Foot of Air. Bar. reading 29 inches.	Diff. for an increase of 10 in Dry	Difference for one inch in Barometer and proportional parts.
60	46 45 44 43 42 41	33'7 31'8 30'0 28'1 26'2 24'3.	-0.4 0.4 0.4 0.4 0.4 0.4	in. 0'193 0'179 0'166 0'154 0'142	in'006 '005 '005 '005 '004'004	gr. 2'2 2'0 1'8 1'7 1'6	0,0 0,0 0,0 0,0 0,0	gr. 3.6 3.8 4.0 4.1 4.2 4.4	gr. +0'3 0'2 0'2 0'2 0'2	37 34 32 30 28 26	- 2 2 2 2 2 - 2	grs. 517'2 '3 '4 '5 '6 517'6	+17.8	17'7 in. grs. '1 1'8 '2 3'5 '3 5'3 '4 7'1
61	61 60 59 58 57 56 55 54 53 52 51 50 49 48 47 46 45 44	61°0 59°1 57°3 55°4 53°5 51°7 49°8 47°9 46°0 44°1 42°3 40°4 38°6 36°7 34°8 33°0 31°1 29°2	-0.8 0.8 0.8 0.8 0.8 0.8 0.8 0.8 0.8 0.8	0'537 0'503 0'470 0'439 0'410 0'383 0'358 0'334 0'311 0'289 0'269 0'250 0'232 0'216 0'201 0'187 0'174 0'161	1017 1016 1014 1013 1012 1011 1010 1009 1008 1007 1006 1005 1005 1005 1005 1005 1005 1005	6.0 5.6 5.2 4.9 4.6 4.3 4.0 3.7 3.5 3.2 3.0 2.8 2.6 2.4 2.3 2.1 1.9	-0'2 0'2 0'2 0'2 0'1 0'1 0'1 0'1 0'1 0'1 0'1 0'1 0'1 0'1	0.0 0.4 0.8 1.1 1.4 1.7 2.0 2.3 2.5 2.8 3.0 3.2 3.4 3.6 3.7 3.9 4.1 4.2	+0'4 0'4 0'4 0'4 0'3 0'3 0'3 0'3 0'3 0'3 0'3 0'3 0'3 0'3	100 94 88 82 77 72 67 62 58 54 50 47 44 41 38 35 32 30	- 66 6 5 5 5 4 4 4 3 3 3 3 3 2 2 2 2 2 2	514.0 '2 '4 '6 514.8 515.0 '2 '3 '5 '6 ·8 515.9 516.0 '1 '2 '3 '4 '5 ·6 ·8 515.9 516.0 '1 '2 '3 '5 ·6 ·8 515.0 '1 ·8 515.0 '1 ·8 515.0 '1 ·8 515.0 '1 '1 ·8 515.0 '1 ·8 515.0 '1 ·8 515.0 '1 ·8 ·8 ·8 ·8 ·8 ·8 ·8 ·8 ·8 ·8	+17.7	'5 8'9 10'6 '7 12'4 '8 14'2 '9 15'9
62	43 42 62 61 60 59 58 57 56 55 54 53 52 51 50 49 48 47 46 45 44 43	27'3 25'5 62'0 60'1 58'3 56'4 54'6 52'7 50'8 49'0 47'1 45'3 43'4 41'5 39'7 37'8 36'0 34'1 32'2 30'4 28'5 26'7	0.6 -0.6 -0.8 0.8 0.8 0.8 0.8 0.8 0.8 0.7 0.7 0.7 0.7 0.7 0.7 0.7 0.7 0.6 0.6 -0.6	0'149 0'138 0'556 0'520 0'487 0'456 0'427 0'399 0'372 0'347 0'323 0'301 0'281 0'262 0'244 0'227 0'211 0'196 0'182 0'169 0'157 0'145	"004 - "004 - "016 "015 "014 "013 "012 "011 "010 "009 "009 "009 "009 "009 "008 "007 "006 "005 "004 "004 - "004	1'7 1'5 6'2 5'8 5'4 5'1 4'7 4'4 4'1 3'9 3'6 3'4 3'1 2'9 2'7 2'5 2'4 2'2 2'0 1'9 1'7	0'0 -0'0 -0'2 0'2 0'2 0'1 0'1 0'1 0'1 0'1 0'1 0'1 0'1 0'1 0'1	4'3 4'5 0'0 0'4 0'8 1'1 1'5 1'8 2'1 2'3 2'6 2'8 3'1 3'3 3'5 3'7 3'8 4'0 4'2 4'3 4'5 4'6	0°2 +0°4 0°4 0°4 0°3 0°3 0°3 0°3 0°3 0°3 0°3 0°3 0°3 0°3	28 26 100 94 88 82 77 72 67 62 58 54 50 47 44 41 38 35 32 30 28 26	- 6 6 5 5 5 4 4 4 3 3 3 3 3 3 2 2 2 2 2	516-6 512-9 513-1 -3 -5 -7 513-9 514-1 -2 -4 -5 -7 -8 514-9 515-0 -1 -2 -3 -4 -5 -7 -8 514-9 515-0	- 1°0 +17°7	
63	63 62 61 60 59 58 57 56 55 54 53 52 51 50 49	63.0 61.2 59.3 57.5 55.6 53.8 51.9 50.1 48.2 46.4 44.5 42.6 40.8 39.0 37.1	-0.8 0.8 0.8 0.8 0.8 0.8 0.7 0.7 0.7 0.7 0.7 0.6 0.6 0.6 0.6 0.6	0°576 0°540 0°506 0°474 0°443 0°414 0°387 0°361 0°337 0°314 0°292 0°272 0°273 0°236 0°220	-*016 '015 '014 '013 '012 '011 '010 '009 '008 '007 '006 '005 '004*004	6.4 6.0 5.6 5.2 4.9 4.6 4.3 4.0 3.7 3.5 3.3 3.0 2.8 2.6	-0.0 0.0 0.0 0.1 0.1 0.1 0.1 0.1 0.1 0.1	0.0 0.4 0.8 1.2 1.5 1.8 2.1 2.4 2.7 2.9 3.1 3.6 3.8 4.0	+0.4 0.4 0.4 0.3 0.3 0.3 0.3 0.3 0.3 0.3 0.3	100 94 88 82 77 72 67 63 59 55 51 47 44 41 38	- 6 5 5 4 4 4 4 4 3 3 3 2 2	511.7	- 1°0 +17°7	*01 0'2 *02 0'4 *03 0'5 *04 0'7 *05 0'9 *06 1'1 *07 1'2 *e8 1'4 *09 1'6

of '	ading Ther- neter.	Temperature of the Dew-point.	Difference for an in- crease of 1° in Dry.	Elastic force of Vapour,	Difference for an in- crease of 10 in Dry.	Vapour in a Cubic Foot of Air.	Difference for an in- crease of 1° in Dry.	Vap. read. to sat. a Cubic Foot of Air.	Difference for an in- crease of 1° in Dry.	Degree of Humi- dity. (Satn.=100.)	Difference for an in-	Weight of a Cubic Foot of Air. Bar. reading 29 inches.	Diff. for an increase of 10 in Dry	Bill of
Dry.	Wet.	Te	E D	Va	G Di	Va Fo	Dii	Cu	Cre	Dedit	Diff	For	Diff.	Diffe inch and parts.
63°	49 48 47 46 45 44	37·1 35·2 33·4 31·6 29·7 27·8	-0.2 0.2 0.2 0.2 0.2	in. 0'220 0'205 0'191 0'178 0'165 0'153	in'004 -'004 -'004'004	gr. 2'4 2'3 2'1 2'0 1'8 1'7	0.0 0.0 0.0 0.0 0.0 0.0 8t.	gr. 4'0 4'1 4'3 4'4 4'6 4'7	gr. +0.2 0.2 0.2 0.2 0.2 +0.5	38 35 33 31 29 27	- 2 2 2 2 2 - 2	grs. 514'1 '2 '3 '3 '4 514'5	+17.7	17.6 in. grs. '1 1.8 '2 3.5 '3 5.3 4 7.0 '5 8.8
64	64 63 62 61 60 59 58 57 56 55 54 53 52 51 50 49 48 47 46	64.0 62.2 60.3 58.5 56.7 54.8 53.0 51.2 49.4 47.5 45.7 43.9 42.0 40.2 38.4 36.6 34.7 32.9 31.1	-0.8 0.8 0.8 0.8 0.8 0.8 0.8 0.7 0.7 0.7 0.7 0.7 0.7 0.7 0.7 0.7 0.6 0.6	0'596 0'560 0'525 0'492 0'461 0'431 0'403 0'376 0'351 0'328 0'366 0'267 0'249 0'232 0'216 0'201 0'187 0'174	-*016 '016 '015 '014 '014 '013 '012 '010 '009 '008 '007 '007 '007 '006 '006 '006 '005 '005	6.6 6.2 5.8 5.4 5.1 4.8 4.5 4.2 3.9 3.6 3.4 3.2 3.0 2.8 2.6 2.4 2.2 2.1 1.9	-0'2 0'2 0'2 0'2 0'2 0'2 0'2 0'1 0'1 0'1 0'1 0'1 0'1 0'1 0'1 0'0 0'0	0°0 0°4 0°8 1°2 1°5 1°8 2°1 2°4 2°7 3°2 3°4 3°6 3°8 4°0 4°2 4°4 4°5 4°7	+0'4 0'4 0'4 0'4 0'4 0'4 0'4 0'3 0'3 0'3 0'3 0'3 0'3 0'3 0'2 0'2	94 88 82 77 72 67 63 59 55 51 48 45 42 39 36 33 31 29	3 2 2 2 2 2	511.9 512.1 .3 .4 .6 .7 512.8 513.0 .1 .2 .3 .4 .5	- 0°9 +17°6	'5 8'8 '6 10'6 '7 12'3 '8 14'1 '9 15'8
65	65 64 63 62 61 60 59 58 57 56 55 54 53 52 51 50 49 48 47 46 45 44	29'2 65'0 63'2 61'4 59'5 57'7 55'9 54'1 52'3 50'4 48'6 46'8 45'0 43'2 41'3 39'5 37'7 35'9 34'1 32'2 30'4 28'6 26'8	-0.6 -0.8 0.8 0.8 0.8 0.8 0.8 0.7 0.7 0.7 0.7 0.7 0.7 0.7 0.7 0.7 0.7	0'162 0'617 0'580 0'544 0'510 0'478 0'447 0'418 0'391 0'366 0'342 0'299 0'279 0'260 0'242 0'225 0'210 0'196 0'182 0'169 0'157 0'146	'004 '016 '016 '015 '014 '013 '012 '011 '010 '009 '009 '009 '009 '005 '005 '005 '004 '004 '003	1.8 6.8 6.4 6.0 5.6 5.3 4.9 4.6 4.3 4.0 3.8 3.5 3.3 3.1 2.9 2.7 2.5 2.3 2.2 2.0 1.9 1.7	-0'0 -0'2 0'2 0'2 0'1 0'1 0'1 0'1 0'1	4.8 0.0 0.4 0.8 1.2 1.5 1.9 2.2 2.5 2.8 3.0 3.3 3.5 3.7 3.9 4.1 4.3 4.5 4.6 4.8 4.9 5.1 5.2	+0'4 0'4 0'4 0'4 0'3 0'3 0'3 0'3 0'3 0'3 0'3 0'3 0'3 0'3	27 100 94 88 83 78 73 68 63 59 55 51 48 45 42 39 36 34 32 29 27 25 23	- 6 6 5 5 5 4 4 4 4 3 3 3 3 2 2 2 2 1 1	513.5 509.5 509.8 510.0 '2 '4 '6 510.8 511.0 '2 '3 '5 '6 ·8 511.9 512.0 '1 '2 '3 '4 '5 '6 512.6	- oʻ9 - oʻ9	17'5 1 1 8 '2 3'5 '3 5'3 '4 7'0 '5 8'8 '6 10'5 '7 12'3 '8 14'0 '9 15'8
66	66 65 64 63 62 61 60 59 58 57 56 55 54	66°0 64°2 62°4 60°6 58°8 57°0 55°1 53°3 51°5 49°7 47°9 46°1 44°3	-0.8 0.8 0.8 0.8 0.8 0.7 0.7 0.7 0.7 0.7 -0.7	0.639 0.601 0.564 0.529 0.496 0.464 0.466 0.380 0.356 0.333 0.311 0.280	-'017 '016 '015 '014 '012 '011 '010 '009 '008 '008 '007 -'006	7.0 6.6 6.2 5.8 5.5 5.1 4.8 4.5 4.2 3.9 3.7 3.4 3.2	-0'2 0'2 0'2 0'1 0'1 0'1 0'1 0'1 0'1 0'1 -0'1 -0'1	0°0 0°4 0°8 1°2 1°5 1°9 2°2 2°5 2°8 3°1 3°3 3°6 3°8	+0.2 0.2 0.2 0.2 0.3 0.4 0.4 0.4 0.4 0.4 0.4 0.4	94 88 83 78 73 68 64 60 56 52 48 45	5 5 4 4 3 3 3 3 3	508.8	+17.5	'01 0'2 '02 0'4 '03 0'5 '04 0'7 '05 0'9 '06 1'1 '07 1'2 '08 1'4 '09 1'6

66	of T mon	ding Ther- neter.	Temperature of the Dew-Point.	Difference for an in- crease of 1° in Dry.	Elastic force of Vapour.	Difference for an in- crease of 1° in Dry.	Vapour in a Cubic Foot of Air.	Difference for an in- crease of 10 in Dry.	Vap. reqd. to sat. a Cubic Foot of Air.	Difference for an in- crease of 1º in Dry.	Degree of Humi- dity. (Satn.=100.)	Difference for an in- crease of 1° in Dry.	Weight of a Cubic Foot of Air. Bar. reading 29 inches.	Diff. for an increase of 10 in Dry	Difference for one inch in Barometer and proportional parts.
66	Dry.	Wet.		_	-		V ₁	9 9	20	A S	Ā병	ig F	P F E	of Di	E E E. C
67 67 66 65;2 0°8 0′622 0′16 6′8 0′2 0′5 0′4 9/4 6 6′6 6′6 6′8 0′34 0′8 0′585 0′16 6′4 0′2 0′9 0′4 88 6 65079 + 17.5 6′6 0′2 0′5 0′4 9/4 6 6′6 6′6 0′8 0′585 0′16 6′4 0′2 0′9 0′4 88 6 65079 + 17.5 6′6 0′2 1′7 0′4 88 6 65079 + 17.5 6′6 0′2 1′7 0′4 88 5 508 1′7 0′438 0′13 5′3 0′2 2′0 0′4 78 5 5′3 0′2 0′4 83 5 508 1′7 0′438 0′13 5′3 0′2 2′0 0′4 78 5 5′3 0′2 0′4 83 0′13 5′5 0′2 0′4 0′4 88 5 508 0′7 0′453 0′12 5′0 0′2 2′3 0′4 0′4 88 5 508 0′7 0′372 0′10 4′4 0′1 3′2 0′3 5′6 0′2 0′7 0′348 0′9 3′8 0′1 3′5 0′2 2′6 0′4 0⁄4 4 508′9 5′5 4′7 0′344 0′0 0′3 0′342 0′0 0′8 0′342 0′0 0′8 0′284 0′08 3′3 0′1 3′5 0′3 52 4 4 5′5 5′5 4′5 0′7 0′324 0′08 3′3 0′1 3′5 0′3 52 4 4 5′5 5′5 4′5 0′7 0′324 0′08 3′3 0′1 3′5 0′3 52 4 4 5′5 5′5 4′5 0′7 0′324 0′08 3′3 0′1 3′5 0′3 52 4 4 5′5 5′5 4′5 0′7 0′325 0′38 3′3 0′1 4′0 0′3 40 3 5′5 0′3 5′5 4′5 0′7 0′284 0′08 3′3 0′1 3′5 0′3 52 4 4 5′5 5′5 4′5 0′7 0′325 0′38 3′3 0′1 4′0 0′3 40 3 5′5 0′3 5′5 4′5 0′7 0′284 0′08 3′3 0′1 4′4 0′3 40 3 5′5 0′2 0′3 0′3 0′28 0′28 0′3 0′3 0′1 4′4 0′3 40 3′3 5′5 0′3 3′4 0′0 0′6 0′247 0′06 2′7 0′1 4′6 0′3 3′3 3′3 5′5 0′1 4′4 0′3 3′4 0′3 0′4 0′4 0′4 0′4 0′4 0′4 0′3 3′4 0′4 0′4 0′4 0′4 0′4 0′4 0′4 0′3 3′4 0′4 0′4 0′4 0′4 0′4 0′4 0′4 0′4 0′4 0	66	54 53 52 51 50 49 48 47 46	42.5 40.7 38.9 37.0 35.2 33.4 31.6 29.8	0.7 0.7 0.6 0.6 0.6 0.6 0.6	0'280 0'271 0'253 0'236 0'220 0'205 0'191 0'178 0'165	coc6 coc6 coc6 coc6 coc6 coc6 coc6	3.5 2.6 2.4 2.3 2.1 2.0 1.8	0.0 0.0 0.1 0.1 0.1 0.1 0.1 0.1	3.8 4.0 4.2 4.4 4.6 4.7 4.9 5.0 5.2	+0.4 0.4 0.4 0.4 0.4 0.4 0.3 0.3	42 40 37 34 32 30 28 26	2 2 2 2 2 2 2 2 2 2 2	510.8 510.9 511.0 2 3 4 55.6	- 0.9	in. grs. 1 1'8 2 3'5 3 5'3 4 7'c 5 8'8 6 10'5 7 12'3 8 14 0
67 66 6 6 2 0 8 0 6 4 0 18 71 0 2 0 4 0 5 94 6 5 6 6 6 6 6 6 6 6 6 6 6 6 6 6 6 6 6	67	66 65 64 63 62 61 60 59 58 57 56 55 54 53 52 54 54 54 54 54 54 54 54 54 54 55 56 56 56 56 56 56 56 56 56 56 56 56	65.2 63.4 61.6 59.8 58.0 56.2 54.4 52.6 50.8 49.0 47.2 45.4 43.6 41.8 40.0 38.2 36.4 34.6 32.8 31.0	0.8 0.8 0.7 0.7 0.7 0.7 0.7 0.7 0.7 0.7 0.7 0.7	0.622 0.585 0.549 0.515 0.483 0.453 0.424 0.397 0.372 0.348 0.325 0.304 0.284 0.265 0.247 0.230 0.214 0.199 0.185 0.172	*016 *016 *015 *014 *013 *012 *011 *010 *010 *009 *008 *008 *008 *008 *008 *007 *006 *005 *004 *003 *003	6.4 6.0 5.6 5.3 5.0 4.7 4.4 4.1 3.8 3.6 3.3 2.7 2.7 2.5 2.4 2.2 2.0	0'2 0'2 0'2 0'2 0'2 0'1 0'1 0'1 0'1 0'1 0'1 0'1 0'1 0'1 0'1	0.5 0.9 1.3 1.7 2.0 2.3 2.6 2.9 3.2 3.5 3.7 4.0 4.2 4.4 4.6 4.8 4.9 5.1 5.3 5.4	0'4 0'4 0'4 0'4 0'4 0'4 0'3 0'3 0'3 0'3 0'3 0'3 0'3 0'3	94 88 83 78 73 68 64 60 56 52 49 46 43 40 37 34 32 30 28 26	6 6 5 5 5 5 5 5 5 5 4 4 4 4 3 3 3 3 3 3 3 2 2 2 2 2	6 507.9 508.1 3 5 7 508.9 509.1 2 4 5 7 8 509.9 510.1 2 3 4 4 5 7 8	-	9 15-8
67 65'4 0'8 0'635 '016 7'3 0'2 0'5 0'4 94 6 4 - '05 0'9		67 66 65 64 63 65 59 57 56 55 57 55 54 57 59 49 48 47 46	66·2 64·4 62·6 60·8 59·1 57·3 55·5 53·7 50·1 48·3 46·5 44·7 42·9 41·2 39·4 37·6 35·8 34·0 32·2 30·4 28·6	0.8 0.8 0.8 0.8 0.7 0.7 0.7 0.7 0.7 0.6 0.6 0.6 0.6 0.6 0.6 0.6 0.6 0.6	0.644 0.606 0.569 0.534 0.501 0.470 0.441 0.413 0.387 0.362 0.339 0.317 0.296 0.276 0.258 0.241 0.225 0.210 0.196 0.182 0.169 0.157	*018 *017 *017 *016 *015 *013 *012 *011 *010 *009 *008 *007 *006 *006 *006 *006 *006 *006 *006	7'1 6'6 6'2 5'8 5'5 5'5 4'8 4'5 4'0 3'7 3'5 3'2 2'8 2'6 2'5 2'3 2'2 2'0 1'7	0'2 0'2 0'2 0'1 0'1 0'1 0'1 0'1 0'0 0'0 0'0 0'0 0'0	0'4 0'9 1'3 1'7 2'0 2'3 2'7 3'0 3'3 3'5 3'8 4'0 4'3 4'5 4'7 4'9 5'0 5'2 5'3 5'5 5'6 5'8	0°5 0°5 0°5 0°5 0°4 0°4 0°4 0°4 0°3 0°3 0°3 0°3 0°3 0°3 0°3 0°3 0°3	94 88 83 78 73 68 64 60 56 52 49 46 43 40 37 35 33 31 29 27 25 23	6 6 5 5 5 5 5 4 4 4 4 3 3 3 3 3 3 2 2 2 2 2 2 2 6	55 506.7 507.0 2 4.6 507.8 508.0 2 3.5 6.6 7 508.9 509.0 1.2 3.3 4.5 6.6 509.6	+17.5	'02 0'4 '03 0'5 '04 0'7

of T mon	ding her-	Temperature of the Dew-Point.	Difference for an in- crease of 1° in Dry.	Elastic force of Vapour.	Difference for an in- crease of 1° in Dry.	Vapour in a Cubic Foot of Air.	Difference for an in- crease of 1° in Dry.	Vap. reqd. to sat. a Cubic Foot of Air.	Difference for an in- crease of 1° in Dry.	Degree of Humidity. (Satn.=100.)	Difference for an in- crease of 10 in Dry.	Weight of a Cubic Foot of Air. Bar. reading 29 inches.	Diff. for an increase of 10 in Dry	Difference for one inch in Barometer and proportional parts.
Dry.	Wet.	- o	0	in.	in.	gr.	gr.	gr.	gr.	G.9	_ G			Diff. and part
69	64	60.1	-0.4	0'547	-'012	5'7	-0'2	2°I	+0.4	73 68	- 4	506.4 grs.	- 0.0	17.4
	63	58.3	0.4	0'457	.010	5.3	0.1	2.2	0.3	64	4	506.8	+17.4	in. grs.
	61	54.8	0.4	0'429	,010	4:7	0.1	3.1	0.3	60	4	5070	1-17	'1 1'7 '2 3'5
	59	23.0	07	0.377	.000	4.4	0,1	3'4	0.3	56	3	1	Belle.	3 5.5
	58	49'4	0.6	0.320	*008	3.6	0.1	3.9	0.3	50	3	.5	1515	'4 7'0 '5 8'7 '6 10'4
	57 56	45'9	0.6	0'309	.007	3.4	0,1	4'2	0.3	47	3	-7	ATOR.	·6 10·4 ·7 12·2
	55	44'1	0.6	0'289	*005	3.5	0,1	4.8	0.3	41	3 2	507'9		-8 13.9
	54	40'5	0.6	0.52	.002	2.8	0.1	2.0	0.3	38	2	208.0	100	9 15.4
	52	38.7	0.6	0'235	*005	2.4	0,1	5'2	0.3	33	2 2	.5	1000	
	51	35.5	0.6	0'204	.002	2.5	0.0	5.4	0.3	31.	2	*3	1379	Ten 3
	49	33.4	0.6	0,130	-'004	2'I 2'0	-0.0	5.8	+0.5	27	- 2	508.6		
70	48	70.0	-0.8	0.177	-,010	8.0	-0.5	0.0	+0.2	100	- 6	MARKET THE PARTY OF THE PARTY O	1	
,0	69	68.2	0.8	0.691	.019	7.5	0'2	0.2	0.2	94	6	504.0	- 0.0	
	68 67	66.5	0.8	0.613	.012	7°1	0'2	0.0	0.2	88	5	504.8	+17.4	
	66	62.9	0.4	0.246	.019	6.3	0'2	1.4	0.2	78	5 5	5050		The same
	65	59.4	0.4	0.241	'015	5.2	0'2	2.1	0.2	73	4	.3	3-3-3	1000
	63	57.6	0.4	0.476	.013	5.5	0.1	2.8	0'4	65	4	.7		100
	62	55.8	0.4	0.446	.010	4.6	0.1	3.1	0.4	61 57	4 3	505.0		
	60	52.3	0.4	0.392	.009	4.3	0,1	3.7	0.4	53	3	.2		
	59 58	50.2	0.4	0.368	.000	3.8	0.1	4'0	0.4	50	3	·4 ·5	TO THE	
	57	47'0	0.6	0.353	.008	3.2	0.1	4.5	0.4	44	2	.7	Jane 1	
	56 55	45'2	0.6	0.305	*007	3.1	0.1	4.7	0'4	38	2 2		100	139.94
	54	41.7	0.6	0.562	.007	2.9	0.1	2.1	0.4	36	2	507.1	10/6	15 19
	53 52	39.3	0.6	0'247	*006	2.2	0.0	5.2	0.4	34	2 2	·2		
	51	36 4	0.6	0'214	.004	2.3	0.0	5.7	0.3	29	2	'4	De la constante de la constant	Tel 1
	50	34.6	-0.2	0,182	003	2.0	-0.0	5.8	+0.3	27	- 1	507.5	132	1000
71	71	71.0	-0.8	0'759	-'020	8.3	-0'2	0.0	+0.4	100	_ 6	502.9	- 0.9	
P	70	69.2	0.8	0'714	.018	7.8	0'2	0.2	0.4	94 88	5	503*2		
	69	65.7	0.8	0.633	.019	7.3	0.5	1'4	0'4	83	5 5	.4	+17.4	1
	67	64.0	0.8	0.596	'015	6.2	0'2	1.8	0.4	78	5	503'9		
	66	60.4	0.7	0.260	'013	5.7	0.1	2.2	0.4	73 69	4 4	504.2	1331	
	64	58.7	0.4	0'494	.011	5.4	0,1 0,1	2.9	0.3	65	4	•6	3 33	
	63	20.0	0.4	0.436	,010	5°1	0.1	3.6	0.3	57	3	504.9	1000	400
	61	53.4	0.7	0.383	.010	4.4	0,1	3'9	0.3	53 50	3 3 2	202,1	1	-
	59	46.9	0.4	0'359	.000	3.9	0.1	4.1	0.3	47	2	.5	1534	19019
	58	48.1	0.6	0.336	,008	3.7	0,1	4.6	0.3	44 41	2 2	-6	1	1 12 100
	57 56	44.6	0.6	0'295	.008	3'4	0,1	4.9	0.3	38	2	505'9	11/2	'01 0'2
	55	42.8	0.6	0'276	*007	3.0	0,1 0,1	5.3	0,3	36	2 2	206.0		.03 0.2
	54 53	39.3	0.6	0'241	.002	2.6	0.1	5'7	0.3	32	2	'2	N THE	.04 07
	52 51	35.8	0.2	0'225	*004	2.2	0.1	5.8	0,3	30	2 2	*3	1 7-31	06 1.0
	50	34'0	0'5	0.196	'003	2'1	0,1	6.2	0'3	26	1	.5		'07 1'2
	49	32.3	0.2	0.120	003	1,0	-0.0	6.4	+0.5	24	- I	506.7	19794	08 1.4

-	-	-			2 .	I a	1 4	d .	1.	1.0	11.	II.	19	
		Temperature of the Dew-Point.	Difference for an in- crease of 1° in Dry.	of o	Difference for an in- crease of 1° in Dry.	Cubic	Difference for an in- crease of 10 in Dry.	Vap. reqd. to sat.	Difference for an in- crease of 1° in Dry.	Degree of Humidity. (Satn. = 100.)	Difference for an in- crease of 1° in Dry.	a Cubic Bar.	Diff. for an increase of 10 in Dry	Difference for one inch in Barometer and proportional parts.
	ding	lo a	in a	force	or or		in l	to s	in or	H	in a	Weight of a Cubi Foot of Air. Bar reading 29 inches.	for an incr 10 in Dry in in Bar.	for
	her- neter.	11 11	r 1º	271	100	9.5	10 Peef	Pd.	To-	of	Lee Lee	of a Air. 29 in	8 8 8	Ban
1		Po-Po	ren e ol	tic nr.	ren	of E	e o	5 A	ren e ol	80	Ten e	ng of	for in	Haring .
1	Tara B	cw c	iffe	Elastic Vapour.	iffe	Vapour Foot of	iffe	e di	Difference for crease of 1° in	egr ity.	iffe	Weight of a Foot of Air.	#	Difference for inch in Baron and proporti parts.
Dry.	Wet.	HA	0.5	MP	0.0	A	52	NO.	H 5	De	85	># 5	of Di	D.E E E
	0	0	0	in.	in.	gr.	gr.	gr.	gr.			grs.	grs.	
72	72	72'0	-0.4	0.785	019	gr. 8 5	-0'2	0.0	+0.2	100	- 6	201.8	- 0.0	17.3
1	71	70'2	0.4	0.696	'017	8°0	0'2	0.0	0.2	94	5	502'1	+ 17.3	in. grs.
1	7º 69	66.7	0.4	0.655	.015	7.1	0,5	1.4	0.2	84	5	·4 ·6	7 -/ 3	'1 1'7
10	68	650	0.4	0.617	'014	6.7	0'2	1.8	0.2	79	4	502'9	Ball Ball	.3 2.2
1	67	63.5	0.7	0.281	'013	6.3	0'2	2.5	0.2	74	4	203.1	100	4 6.9
-	66	61.2	0.4	0.244	.013	5.9	0'2	2.6	0.2	69	4	.4	10	.2 8.4
1	65	59.7	0.4	0.214	'012	5.6	0'2	2.9	0.2	65	4	.6	1	.6 10.4
1	64 63	56.5	0.7	0.454	110,	5.0	0.7	3.2	0'5	57	4 3	503.9		8 13.8
	62	54:5	0.6	0.426	.010	4.7	0,1	3.8	0'4	54	3	204.1		.8 13.8
1	61	52.7	0.6	0.399	.000	4.4	0.1	4.1	0.4	51	3	-3		31.50
1	60	51.0	0.6	0'374	.008	4'1	0,1	4.4	0.4	48	3	.6		10 23 3
	59	49'2	0.6	0.350	*007	3.8	0.1	4.7	0.4	45	3	.6		
1	58	47.5	0.6	0'328	*005	3.9	0.0	4'9 5'2	0.4	42 39	2 2	504.9	1	
	57 56	44.0	0.6	0'287	*005	3.1	0.0	5.4	0.3	36	2	202.0	1	1
1	55	42'2	0.6	0.269	*005	2.9	0.0	5.6	0.3	34	2	.1		1
1	54	40'5	0.6	0'252	*004	2.7	0.0	5.8	0.3	32	2	.3	1	1
	53	38.7	0.6	0'236	*004	2.6	0,0	2.9	0.3	30	2	*4		
1	52	37.0	0.2	0'221	*004	2'4	0,0	6.3	0,3	28	2 I	.6		i
	51 50	33.2	0.2	0,193	*004	2'0	0.0	6.5	0.3	24	i	.6		12
	49	31.8	-0.2	0,180	- '004	1.9	-0.0	6.6	+0.3	23	- 1	505'7		1
				0		0.0								
73	73	73.0	-0.4	0.266	-,018	8.8	-0.3	0.0	+0.2	100	- 6	500.7	- 0.0	
1	72 71	71.3	0.4	0'722	'017	8.3	0'2	0.2	0.2	94 89	5 5	201.0	+17.3	
1	70	67.8	0.7	0.680	.016	7.4	0'2	1.4	0.2	84	5	.5	1-73	
	69	66.0	0.4	0.641	.016	7.0	0'2	1.8	0.2	79	4	501.8		
1	68	64.3	0.4	0.604	.012	6.6	0'2	2.2	0.2	74	4	502'0		
	67	62.6	0.4	0.268	.014	6.5	0'2	2.6	0.2	70	4	.3	160	
1	66	20.1	0.4	0.234	.011	5.8	0'1	3'0	0.4	66	4	.5	90 01	
1	64	57'3	0.6	0.472	.000	2.1	0.1	3.4	0.4	58	3			
	63	55.6	0.6	0.443	*008	4.8	0.1	4.0	0.4	54	3	503.1		
	62	53'9	0.6	0.416	.008	4.5	0.1	4.3	0.4	51	3	'2		
	61	52.1	0.6	0.390	800	4'2	0.1	4.6	0.4	48	3	-4		
1	60	50.4	0.6	0.366	*008	3.7	0,1	4·8	0'4	45	2 2	.5		16 10
	59	46.9	0.6	0.355	*007	3.2	0.1	5'3	0.4	42	2	503.8		100
	57	45'2	0.6	0'302	*007	3.3	0.1	5.2	0.4	37	2	504.0		
1	56	43'4	0.6	0.583	*007	3.1	0.1	5.7	0'4	35	2	.I		
1	55	41.7	0.6	0'265	*007	2.9	0.1	2.9	0.4	32	2	.5		
	54 53	38.5	0.2	0,535	*007	2.2	0.1	6.3	0'4	30	2 2	.3		
	52	36.2	0.2	0'217	.006	2.3	0.0	6.5	0.3	26	1	.4		
	51	34.7	0.2	0'202	.006	2.5	0.0	6.6	0.3	24	1	.6		
1	50	33.0	-0.2	0.188	002	2'0	-0.0	6.8	+0.3	23	- I	504.7		
74.	74	74.0	-0.7	0.840	-'020	9.1	-0'2	0.0	+0.2	100	_ 6	10016	- 0.0	
14	73	72.3	0.7	0.43	.019	8.6	0'2	0.2	40.2	94		499'6	- 0 9	
	72	70'5	0.4	0.748	.018	8.1	0'2	1.0	0.2	89		500.5	+17.2	43
1	71	68.8	0.4	0.705	'017	7.6	0'2	1.2	0.2	84	5	.2		19.1.
	69	65.3	0.4	0.664	.016	7'2	0'2	1.9	0.2	79	5	500.4	134 15	2.3
The same	68	63:6	0.4	0.288	·015	6.8	0'2	2.3	0.2	74		201,0		'01 0'2
1	67	61.9	0.4	0.224	.013	6.0	0'2	3.1	0.2	66	4			'02 0'4
1	66	60'2	0.4	0.255	.013	5.6	0.1	3.2	0.4	62	4	- '5	100	03 0.2
130	65	58.4	0.6	0.492	'012	5'3	0.1	3.8	0.4	58	3	501.9		.02 0.0
1	64	56.7	0.6	0'463	'012	5.0	0.1	4.1	0.4	55	3	502'1		.06 1.0
100	62	55'0	0.6	0.435	,010	4.7	0,1	4'4	0'4	52	3	'2	1	'07 1'2
100	61	21.2	-0.6	0.385	009	4.1	-0.I	4.7	+0'4	48	- 3	502.6		.08 1.4
	-			13					No. of the last of	-				1
							100			-			C	

Readii of The momet	er- ter.	Temperature of the Dew-Point.	Difference for an in- crease of 1° in Dry.	Elastic force of Vapour.	Difference for an in- crease of 1° in Dry.	Vapour in a Cubic Foot of Air.	Difference for an increase of 1° in Dry.	Vap. reqd. to sat. a Cubic Foot of Air.	Difference for an in- crease of 10 in Dry.	Degree of Humidity. (Sath.=100.)	Difference for an in- crease of 1° in Dry.	Weight of a Cubic Foot of Air. Bar. reading 29 inches.	Diff. for an increase of 10 in Dry	Difference for one inch in Barometer and proportional parts.
	61 60 59 58 57 56 55 54 53 52 51	51°5 49°8 48°1 46°3 44°6 42°9 41°1 39°4 37°7 35°9 34°2	-0.6 0.6 0.6 0.6 0.6 0.5 0.5 0.5 0.5	in. 0'382 0'358 0'336 0'315 0'295 0'276 0'258 0'241 0'225 0'210 0'196	in'009 '008 '007 '007 '007 '006 '005 '004 '004 '003'003	gr. 4°1 3°9 3°6 3°4 3°2 3°0 2°8 2°6 2°4 2°3 2°1	-0.0 0.0 0.0 0.1 0.1 0.1 0.1 0.1	gr. 5.0 5.2 5.5 5.7 5.9 6.1 6.3 6.5 6.7 6.8 7.0	gr. +0'4 0'4 0'4 0'4 0'4 0'4 0'3 0'3 0'3 +0'3	45 43 40 37 35 33 31 29 27 25 23	- 2 2 2 2 2 2 2 1 J J 1 1 1	grs. 502.6 .7 502.9 503.0 .1 .2 .3 .4 .5 .6 503.7	grs. - 0'9 +17'2	17°2 in. grs. '1 1'7 '2 3'4 '3 5'2 '4 6'9 '5 8'6 '6 10'3 '7 12'0 '8 13'8 '9 15'5
	75 74 73 72 71 70 66 66 66 66 66 66 66 66 66 65 66 66 65 65	75'0 73'3 71'6 69'8 68'1 66'4 64'7 63'0 61'2 59'5 57'8 56'1 54'4 52'6 50'9 49'2 47'5 45'8 44'0 42'3 40'6 38'9 37'2	-0.7 0.7 0.7 0.7 0.7 0.7 0.7 0.6 0.6 0.6 0.6 0.6 0.6 0.6 0.6 0.6 0.6	0.868 0.820 0.774 0.731 0.690 0.650 0.612 0.576 0.542 0.510 0.479 0.450 0.423 0.373 0.350 0.328 0.377 0.288 0.270 0.253 0.237 0.222	'020 '019 '018 '018 '018 '017 '016 '015 '014 '012 '011 '010 '009 '008 '007 '006 '006 '005 '005 '005	9°4 8°9 8°4 7°9 7°4 7°0 6°6 6°2 5°8 5°5 5°2 4°9 4°6 4°3 4°0 3°8 3°6 3°3 3°1 2°9 2°7 2°6 2°4	-0'2 0'2 0'2 0'2 0'2 0'1 0'1 0'1 0'1 0'1 0'1 0'1 0'1 0'0 0'0	0.0 0.5 1.0 2.4 2.8 3.2 3.6 3.9 4.2 4.5 4.5 5.4 5.4 6.3 6.5 6.7 6.8 7.0	+0.5 0.5 0.5 0.5 0.5 0.5 0.4 0.4 0.4 0.4 0.4 0.4 0.4 0.4 0.4 0.4	100 94 89 84 79 74 70 66 62 58 55 52 49 46 43 40 38 36 33 31 29 27 25	- 6 5 5 5 5 4 4 4 4 3 3 3 3 3 3 3 2 2 2 2 2 1 1 1 1	498.5 498.8 499.1 .4 .6 499.9 500.1 .4 .6 500.8 501.0 .2 .3 .5 .6 .8 501.9 502.1 .2 .3 .4 .5 .5 .5 .5 .5 .5 .5 .5 .5 .5 .5 .5 .5	- 0°9 +17°2	
	76 75 74 73 72 71 70 69 68 67 66 66 65 64 66 65 65 65 65 55 55 55 55 55 55	76.0 74.3 72.6 70.9 69.2 67.4 65.7 64.0 62.3 60.6 58.9 57.2 55.5 53.8 52.1 50.4 48.6 46.9 45.2 43.5 41.8 40.1 38.4 36.7	-0.7 0.7 0.7 0.7 0.6 0.6 0.6 0.6 0.6 0.6 0.6 0.6 0.6 0.6	0'897 0'848 0'801 0'756 0'713 0'672 0'633 0'596 0'561 0'528 0'497 0'468 0'441 0'415 0'390 0'366 0'343 0'322 0'302 0'283 0'265 0'248	'020 '019 '018 '017 '016 '014 '013 '012 '011 '010 .009 '008 '008 '008 '008 '007 '007 '007 '007	9°7 9°2 8°6 8°2 7°7 7°2 6°8 6°4 6°1 5°7 5°4 5°1 4°8 4°5 4°2 3°9 3°7 3°5 3°1 2°9 2°7 2°5 2°3	-0.5 0.5 0.5 0.1 0.1 0.1 0.1 0.1 0.1 0.1 0.1 0.1 0.1	0.0 0.5 1.1 1.5 2.0 2.5 2.9 3.3 3.6 4.6 4.9 5.2 5.5 6.0 6.4 6.6 6.8 7.0 7.2	+0.5 0.5 0.5 0.5 0.4 0.4 0.4 0.4 0.4 0.4 0.4 0.4 0.4 0.4	100 94 89 84 79 75 67 63 59 55 52 49 46 43 38 36 34 32 32 28 26	5 5 4 4	497'7	- 0°9 +17°2	*01 0'2 *02 0'3 *03 0'5 *04 0'7 *05 0'9 *06 1'0
	77 76 75	77°0 75°3 73°6	-0.7 -0.7 -0.7	0°927 0°877 0°829	'021 '019	8.9 6.2	-0.5 -0.5	0.2	+0.2	100 94 89	5	496°3 496°9	+17.1	'07 1'2 '08 1'4 '09 1'6

-	-			13		-		-	-				10	_	-
Par	dina	Temperature of the Dew-point,	Difference for an in- crease of 1° in Dry.	e of	Difference for an in- crease of 10 in Dry.	Cubic	Difference for an in- crease of 1° in Dry.	Vap. reqd. to sat. n Cubic Foot of Air.	Difference for an in- crease of 1º in Dry.	Humi-	Difference for an in-	Weight of a Cubic Foot of Air. Bar. reading 29 inches.	Diff. for an increase of 10 in Dry	Difference for one	inch in Barometer and proportional parts.
10	Ther- neter.	fure of.	lo in	force	e for	lir.	1° in	d. to	1º in	of H	lo ir	Air.	f. for an ince	e fo	Baro
		npera v-poi	erenders of	Elastic Vapour.	eren ise of	Vapour in a (erence se of	ic Fe	erence ise of	Degree of] dity. (Satn.=	erence	ight of ding	for an in	ereth	E E
Dry.	Wet.	Ten	Diff	Ella	Diff	Vap	Diff	Vap	Diff	Deg	Diff	We Foo	Diff	Diff	and parts
0	75	73.6	-0.7	in. 0'829	in. - '019	gr. 8.9	gr. -0'2	gr.	gr. +0°5	89		grs. 496'9	grs. — 0'0		17'1
77	74	71.9	0.4	0.783	.018	8.4	0'2	1.6	0.2	84	- 5 5	497'2	-	in.	grs.
	73	70°2 68°5	0.4	0.439	.017	8.0	0'2	2.0	0.2	79	4	497'8	+17.1	'I	3'4
1	71	66.8	0.4	0.658	*015	7.1	0'2	2.9	0.2	71	4	498.0		.3	6.8 2.1
1	69	63.4	0.4	0.284	.013	6.3	0,1	3.3	0.2	67	4 3	.3		.4	8.6
	68	61.7	0.6	0.220	'012	5.6	0,1 0,1	4.1 4.4	0.4	59 56	3 3 3	498.9		1.6	10'3
	66	58.3	0.6	0.488	.010	5'3	0.1	4.7	0.4	53	3	499,1		1.8	13.7
	65	56.6	0.6	0'459	.000	4.6	0,1	5.1	0'4	50	2 2			6.	15'4
	63	53'2	0.6	0'405	.008	4.3	0,1	5.7	0.4	44	2	.6		1	
1	62	51.2	0.6	0.328	.008	3.9	0,1	9.1 2.3	0.4	38	2 2	·8	1954	-	
1	60	48.1	0.6	0.312	*008	3.6	0,1	6.4	0.4	36	2 2	500'1	MIL	1	
1	59	44'7	0.6	0'295	*006	3.5	0.1	6.8	0.4	34 32	2	.3			1
1	57 56	43.0	0.6	0'276	*005	3.0	0.1	7'0	0'4	30	2	.4		1	
1	55	39.6	0.6	0'243	*005	2.6	0.1	7.4	0'4	26	1	.6	101	-	
1	54	37'9	-0.6	0.558	-*005	2'4	-0.0	7.6	+0.3	24	- 1	500.7			
78	78	78.0	-0°7	0.908	-'021 '019	9'7	-0°2	0.0	+0.2	100	- 5 5	495'2	- 0.9		
1	76	74.6	0.4	0.857	.018	9'2	0'2	1.1	0.2	89	5	495.8	+17.1		
1	75	72.9	0.6	0.810	°017	8.7	0.5	1.6	0,2	84 79	5 4	496.1	133		3
	73	69.5	0.6	0.722	'015	7.8	0'2	2.2	0.2	75	4	.7	199		
	72 71	66.1	0.6	0.681	°015	7'3	0.5	3'0	0,2	67	4	496.9			1
	70 69	64.4	0.6	0.602	'013	6.2	0,1	3.8	0'4	63	3	.4		!	
	68	61.1	0.6	0.239	,013	5.8	0.1	4'5	0'4	59 56	3	497.8			
	67	59°4 57°7	0.6	0.208	'012	2,2	0.1	4.8 5.5	0.4	53	3	498.0		-	-
1	65	56.0	0.6	0'449	,010	4.8	0.1	5.2	0'4	47	3	.4		7	
	64	54.3	0.6	0'422	*009	4.3	0.1	5.8	0'4	44	3 2	·5		1	. 1
	62	50.0	0.6	0.323	*008	4.0	0,1	6.3	0.4	39		498.8			
1	60	49'2	0.6	0.358	*006	3.2	0.1	6.8	0'4	37	2	499'0		74.7	1
	59	45.8	0.6	0.308	*006	3,3	0.1	7'0	0'4	32	2 2	·3	TRA		1
	57	42.4	0.6	0'271	*006	2.9	0.1	7'4	0'4	28	1	.5	103		
	56	39.0	-0.2	0.524	-005	2.2	-0.0	7.6	+0.3	27	- 1	499'7			1
79	79	79.0	-0.7	0.990	-'022	10.6	-0'2	0.0	+0.6	100	100	494'1	- 0.9		1
	78	77.3	0.7	0.887	'021 '020	10.1	0'2	0.2	0.6	95	5	.5	-		1
	76	73.9	0.7	0.839	'019	9.0	0.5	1.6	0.6	90	5	494.8	+17.0		
	75 74	72.3	0.7	0'793	,018	8.2	0'2	2.1	0.6	80	4	'4	241		1
	73	68.9	0.4	0.707	'017	7.6	0'2	3'0	0.6	75	4	495'9	2 70	30	1
1	72 71	65.2	0.4	0.666	.012	7°2 6.8	0'2	3.4	0.6	67	4	496.2	133	'OI	0'2
1	70	63.8	0.6	0.592	'014	6.4	0'2	4'2	0.6	59	3	.6	270 9	103	0.2
	68	60'4	0.6	0.228	,013	5.6	0.1	4.6	0.2	56	3	496.8	4++	°04	0.4
	66	58.7	0.6	0.495	'012	5.3	0.1	5'3	0.2	50	3	.5	155	.06	1.0
100	65	55'4	0.6	0.439	,010	5.0	0.1	5.6	0.2	47	3	.4	100	·07	1'4
	64	53'7	-0.6	0.413	009	4.4	-0.1	6.5	+0.2	42	- 3	497.8	1 11 1	.09	1.2
-			-			-					-	-	0.2		

Reaching	-	-	1 0	14.	Jo Of	Té.	II o	1 6 .	4 .	1 4 .	ILIO	Tè.	lo -	12	1.00	_
	Re	ading	of th	r an i		r an i		r an i	sat.	n Dry	Humi = 100.	ramin n Dry	Cubic Bar,	J	r one	tional
	of '	Ther-	ature	f 1º i	THE REAL PROPERTY.	f 1º i	A.E.	fl° ii	qd. to	ree for	of th.	r 1º ir	of a Air.	an in n Dr	Baron	obort
	-	7.99	mper w-Pc	feren	pour	feren	pour ot of	feren	p. re	Teren ase of	gree 7. (S	Teren	ight or of	f. for	eren in	- C
79 64 5377 -076 0431 -1000 474 -071 672 -1075 42 -3 4978 -1076 62 5370 076 07383 1008 379 071 677 075 377 249871 +1770 1776 1776 07343 1708 377 071 679 075 377 249871 +1770 278 378 4876 076 07343 1708 377 071 074 074 388 1 16 178 17	Dry.	Wet.	Teg	G Die	- Ka	Ge	Va Fo	Cre	Cu	ig a	D D D	Cre	Food read	Diff	Dir	part
63 \$200 016 00388 1008 422 011 644 015 39 \$2 49579 \$100 662 662 6036 016 01365 1008 379 011 667 015 37 \$2 49579 \$1170 \$15 611 \$177 \$15 617		64	53.7	-0.6	0'413				6.5	gr. +0°5	42	- 3	grs.			
661	1	63	52'0	1000000	0.388			925200	6.4	0.2	39	2	497'9	-	in.	grs.
So		61	48.6	0.6	0.343	.008	3'7	0.1	6.9	0.2	35	700		+17.0	0.000	
S		1000000	700 00 000	1000				- DECEMBER					.3			5'I
S	13	58	43'5	0.2	0'283	.005	3.0	275000	7.6	0.4	28	1		PR B	.5	
So		56				002	10000	100000000			100000	1/0	498.8		and the same of	10'2
79 78'3 0'7 0'968 '021 10'4 0'2 0'6 0'5 95 5 44 7 7 7 7 7 0 0'7 0'916 0'020 0'8 0'19 0'3 0'2 1'7 0'5 96 5 5493'7 1170 0'7 7 7 7 7 7 7 7 7 7	80	80		-0.7	1'023	023	11.0	-0'2	0.0	+0.2	100	- 5	493'0	- 0.0	.8	13.6
77		79	78.3	0.4	0.016	'021		100000000	10000000	0.2	95	5	*4	-	71	33
76		77	750	0.4	0.867	.019		15 12 1		0.2	85		494'0	+17.0		
74 69'9 0'6 0'732 '016 7'8 0'2 3'2 0'5 7'1 4 94'8 73 68'2 0'6 0'650 '015 7'4 0'2 3'6 0'5 6'7 4 495'1 72 66'5 0'6 0'650 '013 70 0'2 4'0 0'5 6'3 71 64'9 0'6 0'613 '012 6'6 0'2 4'4 0'5 59 69 61'5 0'6 0'558 '011 6'2 0'2 4'4 0'5 69 61'5 0'6 0'545 '011 6'2 0'2 4'8 0'5 56 8 59'8 0'6 0'545 '011 5'2 0'1 5'8 0'1 5'2 0'4 66 56'4 0'6 0'545 '011 5'2 0'1 5'8 0'1 5'2 0'4 66 56'4 0'6 0'545 '011 5'2 0'1 5'8 0'4 66 56'4 0'6 0'455 '010 4'9 0'1 6'1 0'4 44 2 6'6 65 54'8 0'6 0'455 '010 4'9 0'1 6'1 0'4 44 2 6'6 65 54'8 0'6 0'350 '049 0'1 0'1 6'1 0'4 44 2 16 64 53'1 0'6 0'350 '094 1'0 1' 6'9 0'4 37 2 497'0 62 49'7 0'6 0'357 '008 3'8 0'1 7'2 0'4 35 2 2 61 48'0 0'6 0'355 '057 3'4 0'1 7'6 0'4 31 1 1 4 58 43'0 0'5 0'378 '056 3'0 0'1 8'0 0'4 29 1 1 6 58 43'0 0'5 0'378 '066 3'0 0'1 8'0 0'4 29 1 1 6 58 43'0 0'5 0'378 '066 3'0 0'1 8'0 0'4 29 1 1 6 58 43'0 0'5 0'378 '066 3'0 0'1 8'0 0'4 29 1 1 6 58 43'0 0'5 0'378 '063 3'0 0'1 8'0 0'4 29 1 1 6 58 43'0 0'5 0'378 '063 3'0 0'1 8'0 0'4 3' 25 1 1 1 4 58 79'3 0'7 1000 '022 10'7 0'2 0'6 0'6 8'5 492'2 79 77'7 0'7 0'897 '020 9'5 0'2 1'8 0'6 8'5 492'2 79 77'7 0'7 0'897 '020 9'5 0'2 1'8 0'6 8'5 493'1 74 66'3 0'6 0'802 '018 8'6 0'2 2'7 0'6 6'6 8'5 493'1 75 67'6 0'6 0'65 0'75 '014 7'2 0'1 4'1 0'5 0'4 31 1 1 4 76 72'6 0'6 0'802 '018 8'6 0'2 2'7 0'6 0'6 8'5 493'1 76 72'6 0'6 0'6 0'75'7 '016 8'1 0'2 1'2 0'6 90 6'72 493'1 77 74'3 0'7 0'849 0'19 9'1 0'2 2'2 0'6 8'0 4 493'1 74 66'3 0'6 0'75'7 '016 8'1 0'2 1'2 0'6 90 6'72 493'1 75 67'9 0'6 0'75'7 '016 8'1 0'2 1'7 0'5 64 3 12 17'0 6'9 6'9 0'9 0'9 0'9 0'9 0'9 0'9 0'9 0'9 0'9 0		76			THE RESERVE TO STATE OF THE PARTY OF THE PAR	1000000		3000000			80			1		
72 6665 0-60 0-650 0-13 70 0-12 4-0 0-5 63 3 3 0-3 70 0-12 6-60 0-2 4-4 0-15 59 3 0-6 0-6 0-6 0-6 0-6 0-15 8 0-12 6-6 0-2 4-4 4 0-15 59 3 0-6 0-6 0-6 0-6 0-6 0-6 0-6 0-6 0-6 0-6	1	74	69.9	0.6	0'732	.019	7.8	0'2	3'2	0.2	71	4	494.8			1
71 64'9 0'6 0'613 '012 6'6 0'24 4'4 0'5 59 3 16 6 0'578 '011 6'2 0'2 4'8 0'5 56 3 495'8 6 6 0'578 '011 6'2 0'2 4'8 0'5 56 3 495'8 6 6 0'578 '011 6'1 5'8 0'1 5'2 0'4 50 3 12 12 16'6 0'483 '101 5'2 0'1 5'5 0'4 50 3 12 14 11 11 11 0'1 0'1 11 0'1 0'1 11 0'1 0'1			66.2	- W/ 32	0.650			270								
69		71	64.9		0.613	*012	6.6	1000000	4'4	0.2	59	3	.6			
68			61.2	0.6				00/10/03		ACCOUNT OF THE PARTY OF		3	495.0	177		
66					0.4831				5.2			3		-		
64 53:1 0:6 0:404 0:10 4:3 0:1 6:7 0:4 39 2 496:9 6:2 49:7 0:6 0:380 0:09 4:1 0:1 6:9 0:4 37 2 497:9 6:0 6:2 49:7 0:6 0:385 0:07 3:6 0:1 7'4 0:4 33 2 2:2 2:0 6:1 48:0 0:6 0:335 0:07 3:6 0:1 7'4 0:4 33 2 2:2 2:0 6:0 4:7 0:5 0:296 0:007 3:2 0:1 7'8 0:4 29 1 1:6 1:5 0:		66	56.4	0.6	0.455	.010	4'9	37.02	6.1	0.4	44	2	.6			
63 51'4 0'6 0'380 1009 4'1 0'1 6'9 0'4 37 2 497'0 62		65		The second second		A STATE OF THE PARTY OF		100000000000000000000000000000000000000						THE P		
61		63	51'4	0.6	0.380	'009	4'1	0.1	6.9	0.4	37	2	497'0	315		
60		10000	49'7	100000000000000000000000000000000000000		- BATTER 1	3.6	13110	100000000000000000000000000000000000000							1
S8		12,000	46.3		0.312		3'4		7.6	100000	31		.4			
St St St St St St St St		58	43'0		0.278	*006	3.0	0.00	8.0	100000	27		.7			
80		57	41.3	-0.2	0.261	006	2.8	-0.0	8.5	+0.3	25	- 1	497.8	2 10		
79 77.7 0.7 0.947 0.21 10.1 0.2 1.2 0.6 90 5 5 5 5 1.5 +17.0 7.8 76.0 0.7 0.897 0.20 9.5 0.2 1.8 0.6 85 4 492.8 7.7 74.3 0.7 0.849 0.19 9.1 0.2 2.2 0.6 80 4 493.1 76 72.6 0.6 0.802 0.18 8.6 0.2 2.7 0.6 76 4 0.4 7.5 70.9 0.6 0.757 0.16 8.1 0.2 2.3 2.0 6.6 80 4 493.1 7.4 69.3 0.6 0.757 0.16 8.1 0.2 2.3 2.0 6.6 7.2 4 493.7 7.4 69.3 0.6 0.757 0.15 7.6 0.1 3.7 0.5 68 4 494.0 73 67.6 0.6 0.6575 0.14 7.2 0.1 4.1 0.5 64 3 0.2 7.2 65.9 0.6 0.637 0.13 6.8 0.1 4.5 0.5 60 3 0.5 7.1 64.2 0.6 0.601 0.13 6.4 0.1 4.9 0.5 56 3 7.7 7.0 62.6 0.6 0.507 0.13 6.4 0.1 4.9 0.5 5.3 3.4 94.9 9.6 60.9 0.6 0.503 0.11 5.4 0.1 5.9 0.5 53 3.4 94.9 9.6 60.9 0.6 0.503 0.11 5.4 0.1 5.9 0.5 4.7 2 0.3 4.9 9.9 6.6 6.5 5.8 0.6 0.445 0.08 4.8 0.1 6.5 0.5 4.1 2 0.6 6.5 6.5 5.4 2 0.6 0.419 0.08 4.5 0.1 6.5 0.5 4.1 2 0.6 6.5 6.5 5.4 2 0.6 0.419 0.08 4.8 0.1 6.5 0.5 4.1 2 0.6 0.3 5.8 0.6 0.349 0.07 4.2 0.1 7.1 0.5 3.7 2 496.0 6.3 50.8 0.6 0.349 0.07 4.2 0.1 7.1 0.5 3.7 2 496.0 6.3 50.8 0.6 0.349 0.07 4.2 0.1 7.1 0.5 3.7 2 496.0 6.3 50.8 0.6 0.349 0.07 4.2 0.1 7.1 0.5 3.7 2 496.0 6.3 50.8 0.6 0.349 0.07 4.2 0.1 7.1 0.5 3.7 2 496.0 6.3 50.8 0.6 0.349 0.07 3.7 0.1 7.6 0.5 3.3 2 0.3 1.2 0.6 0.5 2.9 2 0.5 5.5 0.3 0.5 0.3 0.5 5.9 44.1 0.5 0.289 0.07 3.7 0.1 7.8 0.5 3.1 2 0.4 0.5 0.5 0.3 0.5 0.5 0.3 0.5 0.5 0.3 0.5 0.5 0.5 0.5 0.5 0.5 0.5 0.5 0.5 0.5	81		300000000000000000000000000000000000000		THE RESERVE AND PARTY.	200	Market Land	10000						- 0.9		
77		79	77'7		0.947	CANAL STREET	THE REAL PROPERTY.	50.00	1'2	0.6	90	5	.2	+17.0		
76		The state of the s	The Party of the last of the l		0.840	120000000000000000000000000000000000000		N. 10000000						723		
74 69'3 0'6 0'715 0'15 7'6 0'1 3'7 0'5 68 4 494'0 73 67'6 0'6 0'6 0'675 0'14 7'2 0'1 4'1 0'5 64 3 72 65'9 0'6 0'637 0'13 6'8 0'1 4'5 0'5 60 3 71 64'2 0'6 0'601 0'13 6'4 0'1 4'9 0'5 56 3 70 62'6 0'6 0'567 0'13 6'0 0'1 5'3 0'5 53 3 494'9 69 60'9 0'6 0'534 0'12 5'7 0'1 5'6 0'5 50 3 494'9 68 59'2 0'6 0'503 0'11 5'4 0'1 5'9 0'5 47 2 67 57'5 0'6 0'445 0'08 4'8 0'1 6'2 0'5 44 2 66 55'8 0'6 0'445 0'08 4'8 0'1 6'5 0'5 44 2 66 55'8 0'6 0'445 0'08 4'8 0'1 6'5 0'5 41 2 66 55'8 0'6 0'445 0'08 4'8 0'1 6'5 0'5 41 2 66 55'8 0'6 0'419 0'08 4'5 0'1 6'8 0'5 39 2 66 45'2 0'6 0'394 0'07 4'2 0'1 7'1 0'5 37 2 67 67 57'5 0'6 0'394 0'07 4'0 0'1 7'3 0'5 35 2 61 47'5 0'6 0'349 0'07 3'7 0'1 7'6 0'5 33 2 62 49'1 0'6 0'349 0'07 3'7 0'1 7'6 0'5 33 2 61 47'5 0'6 0'388 0'07 3'3 0'1 8'0 0'5 29 2 62 49'1 0'6 0'349 0'07 3'7 0'1 7'6 0'5 33 2 61 47'5 0'6 0'328 0'07 3'3 0'1 8'0 0'5 29 2 62 49'1 0'5 0'289 0'07 3'1 0'1 8'2 0'5 27 1 62 49'1 0'5 0'289 0'07 3'1 0'1 8'2 0'5 27 1 63 59 44'1 0'5 0'289 0'07 3'1 0'1 8'2 0'5 27 1 64 496'7 0'04 0'7 0'7 0'978 0'271 -006 2'9 -0'0 8'4 +0'4 26 - 1 496'7 82 82 82 82'0 -0'7 1'031 0'24 11'1 0'3 0'6 0'6 95 5 491'1 83 80'3 0'7 1'033 0'24 11'1 0'3 0'6 0'6 95 5 491'1 84 82 82 82'0 -0'7 1'091 -0'25 11'7 -0'3 0'6 0'6 95 5 491'1 85 78'7 0'7 0'978 0'23 10'5 0'3 1'2 0'6 90 5		76	72.6	0.6	0.802	.018	8.6	0'2	2.7	0.6	76	4	'4	100		
73 67.6 0.6 0.675 0.14 7.2 0.1 4.1 0.5 64 3 2.2 65.9 0.6 0.637 0.13 6.8 0.1 4.5 0.5 60 3 .5 7 7 1 64.2 0.6 0.601 0.13 6.4 0.1 4.9 0.5 5.6 3 494.9 69 60.9 0.6 0.534 0.12 5.7 0.1 5.6 0.5 50 3 495.1 68 59.2 0.6 0.503 0.1 5.4 0.1 5.9 0.5 44 2 0.5 66 5.8 0.6 0.445 0.08 4.8 0.1 6.5 0.5 44 2 0.5 66 5.8 0.6 0.445 0.08 4.8 0.1 6.5 0.5 44 2 0.5 66 5.4 0.6 0.419 0.08 4.8 0.1 6.5 0.5 31 2 495.8 64 52.5 0.6 0.394 0.07 4.2 0.1 7.1 0.5 3.7 2 496.0 63 50.8 0.6 0.311 0.07 4.0 0.1 7.3 0.5 3.5 2 0.1 6.2 49.1 0.6 0.328 0.07 3.7 0.1 7.6 0.5 3.3 2 496.0 62 49.1 0.6 0.328 0.07 3.5 0.1 7.8 0.5 3.1 2 4.1 0.5 0.289 0.07 3.1 0.1 8.0 0.5 2.9 2 0.5 5.5 0.3 0.5 5.8 44.1 0.5 0.289 0.07 3.1 0.1 8.0 0.5 2.9 2 0.5 5.0 0.5 0.3 44.1 0.5 0.289 0.07 3.1 0.1 8.2 0.5 2.7 1 0.6 0.30 0.5 0.5 0.5 0.3 44.1 0.5 0.289 0.07 3.1 0.1 8.2 0.5 2.7 1 0.6 0.30 0.5 0.5 0.9 44.1 0.5 0.289 0.07 3.1 0.1 8.2 0.5 2.7 1 0.6 0.30 0.5 0.3 0.5 0.5 0.5 0.5 0.5 0.5 0.5 0.5 0.5 0.5			2 4 1			100000000000000000000000000000000000000		70.00		100000000000000000000000000000000000000				231		
71		73	67.6	0.6	0.675	'014	7'2	0.1	4'1	0.2		3	'2	1996		
70 62.6 0.6 0.567 0.13 6.0 0.1 5.3 0.5 53 3 494.9 69 60.9 0.6 0.534 0.12 5.7 0.1 5.6 0.5 50 3 495.1 68 59.2 0.6 0.503 0.11 5.4 0.1 5.9 0.5 47 2 3 66 55.8 0.6 0.445 0.08 4.8 0.1 6.5 0.5 44 2 .5 65 54.2 0.6 0.419 0.08 4.5 0.1 6.8 0.5 39 2 495.8 64 52.5 0.6 0.349 0.07 4.0 0.1 7.3 0.5 33 2 .1 62 49.1 0.6 0.349 0.07 3.7 0.1 7.6 0.5 33 2 .3 61 47.5 0.6 0.328 0.07 3.3	- 83	-			0.601											
68 59'2 0'6 0'503 'OII 5'4 0'I 5'9 0'5 47 2 '3 67 57'5 0'6 0'473 '009 5'I 0'I 6'2 0'5 44 2 '5 66 55'8 0'6 0'445 '008 4'8 0'I 6'5 0'5 4I 2 '6 65 54'2 0'6 0'419 '008 4'5 0'I 6'8 0'5 39 2 495'8 64 52'5 0'6 0'394 '007 4'2 0'I 7'I 0'5 37 2 496'0 63 50'8 0'6 0'349 '007 3'7 0'I 7'6 0'5 33 2 '3 61 47'5 0'6 0'328 '007 3'3 0'I 8'0 0'5 31 2 '4 60 45'8 0'6 0'308 '007 3'I 0'I 8'2 0'5 27 I '6 59 44'I 0'5			62.6			.013	6.0							1919		
65 54'2 0'6 0'419 'co8 4'5 0'1 6'8 0'5 39 2 495'8 64 52'5 0'6 0'394 'co7 4'2 0'1 7'1 0'5 37 2 496'0 63 50'8 0'6 0'371 'co7 4'0 0'1 7'3 0'5 35 2 '1 62 49'1 0'6 0'349 'co7 3'7 0'1 7'6 0'5 33 2 '3 61 47'5 0'6 0'328 'co7 3'5 0'1 7'8 0'5 31 2 '4 60 45'8 0'6 0'308 'co7 3'3 0'1 8'0 0'5 29 2 '5 59 44'1 0'5 0'289 'co7 3'1 0'1 8'2 0'5 27 1 6'6 58 42'4 -0'5 0'271 -'co6 2'9 -0'0 8'4 +0'4 26 - 1 496'7 82 82 82'0 -0'7 1'033 'c24 11'1 0'3 0'6 0'6 95 5 491'1 80 78'7 0'7 0'978 'c23 10'5 0'3 1'2 0'6 90 5 5 491'1 80 78'7 0'7 0'978 'c23 10'5 0'3 1'2 0'6 90 5 5 491'1 10 0'2 112 10 0'1 0'2 112 113 0'3 0'6 0'6 95 5 491'1 114 0'3 0'6 0'6 90 5 5 491'1 115 0'3 0'6 0'6 90 5 5 491'1 116'9 '08 1'4		68							5'9	0.2			.3	Provide S		
65 54'2 0'6 0'419 'co8 4'5 0'1 6'8 0'5 39 2 495'8 64 52'5 0'6 0'394 'co7 4'2 0'1 7'1 0'5 37 2 496'0 63 50'8 0'6 0'371 'co7 4'0 0'1 7'3 0'5 35 2 '1 62 49'1 0'6 0'349 'co7 3'7 0'1 7'6 0'5 33 2 '3 61 47'5 0'6 0'328 'co7 3'5 0'1 7'8 0'5 31 2 '4 60 45'8 0'6 0'308 'co7 3'3 0'1 8'0 0'5 29 2 '5 59 44'1 0'5 0'289 'co7 3'1 0'1 8'2 0'5 27 1 6'6 58 42'4 -0'5 0'271 -'co6 2'9 -0'0 8'4 +0'4 26 - 1 496'7 82 82 82'0 -0'7 1'033 'c24 11'1 0'3 0'6 0'6 95 5 491'1 80 78'7 0'7 0'978 'c23 10'5 0'3 1'2 0'6 90 5 5 491'1 80 78'7 0'7 0'978 'c23 10'5 0'3 1'2 0'6 90 5 5 491'1 10 0'2 112 10 0'1 0'2 112 113 0'3 0'6 0'6 95 5 491'1 114 0'3 0'6 0'6 90 5 5 491'1 115 0'3 0'6 0'6 90 5 5 491'1 116'9 '08 1'4			57.5		The second second								.6			
63		65	54'2	0.6	0.419	1008	4.2	0.1	6.8	0.2	39	2	495.8	1773		
62 49'1 0'6 0'349 'co7 3'7 0'1 7'6 0'5 33 2 '3 61 47'5 0'6 0'328 'co7 3'5 0'1 7'8 0'5 31 2 '4 59 44'1 0'5 0'289 'co7 3'1 0'1 8'2 0'5 27 1 '6 58 42'4 -0'5 0'271 -'co6 2'9 -0'0 8'4 +0'4 26 -1 496'7 81 80'3 0'7 1'033 'co24 11'1 0'3 0'6 0'6 95 5 490'8 80 78'7 0'7 0'978 'co23 10'5 0'3 1'2 0'6 90 5 491'1 80 78'7 0'7 0'978 'co23 10'5 0'3 1'2 0'6 90 5 5 491'1		63					100000000000000000000000000000000000000	2000		0.2				1		1
60 45'8 0'6 0'308 '007 3'3 0'1 8'0 0'5 29 2 5 5 44'1 0'5 0'289 '007 3'1 0'1 8'2 0'5 27 1 '6 496'7 58 42'4 -0'5 0'271 -'006 2'9 -0'0 8'4 +0'4 26 -1 496'7 -0'8 0'5 0'9	-	62	49'1	0.6	0'349	*007	3.7	0.1	7.6	0.2	33			THE PERSON NAMED IN	·orl	0'2
82 82 82·0 -0·7 1·091 -·025 11·7 -0·3 0·6 0·6 95 5 491·1 -0·8 1·2 1·2 1·3 1·4		2000			0.308	and the second second		THE RESERVE OF THE PARTY OF THE	8.0	0.2	29	300	.5	21/3	'02	0.3
82 82 82.0 -0.7 1.091025 11.7 -0.3 0.0 +0.6 100 - 2 490.8 - 0.8 1.0 1.0 1.0 1.0 1.0 1.0 1.0 1.0 1.0 1.0		59	44'1	0.2	0.588	'007	3.1	0,1	8.2	0.2	27			100		
81 80·3 0·7 1·033 ·024 11·1 0·3 0·6 0·6 95 5 491·1 80 78°7 0·7 0·978 ·023 10·5 0·3 1·2 0·6 90 5 ·5 +16·9 ·08 1·4	2-	100	10000									999		- 0.8	05	0'9
1 80 787 0.7 0.978 .053 10.2 0.3 1.7 0.6 0.0 2 .2 +10.0 08 1.4	02	81	80.3	0.4	1.033			0.3	0.6	0.6	100000000000000000000000000000000000000	5	491'1		.07	1.2
		22.02			0'978							- 5		+10.9		
		19	"	1	0 920	022	99	3	10		-3	-1				

of T mom	ding her- leter.	Temperature of the Dew-Point,	Difference for an in- crease of 1° in Dry.	Elastic force of Vapour,	Difference for an in- crease of 1° in Dry.	Vapour in a Cubic Foot of Air,	Difference for an in- crease of 1° in Dry.	Vap. reqd. to sat. a Cubic Foot of Air.	Difference for an in- crease of 1° in Dry.	Degree of Humidity. (Satn. = 100.)	Difference for an in- crease of 1° in Dry.	Weight of a Cubic Foot of Air. Bar. reading 29 inches.	Diff. for an increase of 1 in. in Bar.	Difference for one inch in Barometer and proportional parts.
82	79 78 77	75°3 73°6	-0.4 0.6 0.6	in. 0'926 0'877 0'830	in. - '022 '021 '020	gr. 9'9 9'4 8'9	gr. -0'3 0'3	gr. 1'8 2'3 2'8	gr. +0.6 0.6	85 80 76	- 5 4 4	grs. 491'8 492'1	+16.9 - 0.8	16.9 in. grs.
	76 75 74 73	72.0 70.3 68.6 67.0	0.6 0.6 0.6	0.785 0.742 0.701 0.662 0.624	*019 *017 *016	8·4 7·9 7·5 7·1	0'2 0'2 0'2	3°3 3°8 4°2 4°6	0.2	72 68 64 60	4 4 3 3	492.7 493.0 2		'2 3'4 '3 5'1 '4 6'8 '5 8'5 '6 10'1
	72 71 70 69 68	65.3 63.6 62.3	0.6	0.24 0.24 0.254 0.254 0.492	'014 '013 '012 '011	6·7 6·3 5·9 5·6 5·2	0'2 0'2 0'2 0'1	5°0 5°4 5°8 6°1 6°5	0°5 0°5 0°5 0°4	57 54 51 48 45	3 3 3 3 3	493'9 494'1		.6 10.1 .2 11.8 .8 13.2
	67 66 65 64	20.9 20.9 20.9	0.6	0.464	.008 .008	4.9 4.4 4.1	0,1 0,1 0,1 0,1	6·8 7·0 7·3 7·6	0'4 0'4 0'4	42 40 38 35	2 2 2 2	494.8 495.0		
	63 62 61 60	50°2 48°6 46°9 45°2	0.2 0.2 0.9	0'364 0'342 0'321 0'301	*008 *007 *006	3'9 3'6 3'4 3'2	0.1 0.1 0.1 0.1	7.8 8.1 8.3 8.5	0'4 0'4 0'4	33 31 29 27	2 1 1	·3 ·5 ·6		
83	59 83 82 81	43°5 83°0 81°3	-0.2 -0.4 0.7 0.6	0°282 1°127 1°067 1°010	-'005 -'023 '022	3°0 11'7 10'8	0.3 0.3 -0.3	8·7	+0°4 +0°7 0°7 0°7	26 100 95 90	- 5 5	495.8 489.6 490.0	+ 16·9 - 0·8	
	80 79 78 77	79°7 78°0 76°3 74°7 73°0	0.6	0.956 0.856 0.856	'019 '018 '017	9'7 9'1 8'6	0.2	1.8 2.3 2.9 3.4	0.6	85 80 76 72	5 4 4 4	490.7 491.0 3	+109	
	76 75 74 73	71.3 69.7 68.0 66.3	0.6 0.6 0.6	0.766 0.724 0.684 0.646	'015 '014 '013 '012	8·2 7·7 7·3 6·9	0'2 0'2 0'2	3.8 4.3 4.7 5.1	0.6 0.6 0.6	68 64 60 57	4	491.8 492.1 .4 .6		
	72 71 70 69	64.7 63.0 61.3 59.7	0.6	0.610 0.576 0.543 0.512	'012 '012 '011	6·5 6·1 5·8 5·4	0.5 0.5 0.1	5°5 5°9 6°2 6°6	0.6 0.6 0.6	54 51 48 45	3 2 2	492°9 493°1 °3 °5 •6		
	68 67 66 65	58.0 56.3 54.7 53.0	0.6 0.6 0.6	0'482 0'454 0'428	.009 .009	5°1 4°8 4°6 4°8	0.1 0.1 0.1	6·9 7·2 7·4 7·7	0.2	42 40 38 36	2	493.8 494.0		
	64 63 62 61 60	51°3 49°7 48°0 46°3 44°7	0.2 0.2 0.2 0.2	0'379 0'356 0'315 0'396	*008 *007 *007 *007	3.8 3.8 3.8	-0.1 0.1 0.1 0.1 0.1	8.0 8.2 8.4 8.7 8.9	0.2 0.2 0.2 0.2	34 32 30 28 26	2 1 1 - 1	*3 *4 *6 *7 494*8		
84	84 83 82	84°0 82°3 80°7	-0.6 0.6 0.6	1.164 1.103 1.042	-'023 '021 '019	12.4 11.7 11.1	-0.3 0.3	0.0	+0.7	100 95 90	- 5 5 5	488·4 488·8 489·2	+ 16·9 - 0·8	
	81 80 79 78 77	79°0 77°4 75°7 74°0 72°4	0.6 0.6 0.6	0.990 0.938 0.888 0.840 0.794	'017 '016 '015 '014 '013	10°5 10°0 9°4 8°9 8°5	0'2 0'2 0'2 0'2	1.9 2.4 3.0 3.5 3.9	0.6 0.6 0.6	85 80 76 72 68	4	489°9 490°2		
277	76 75 74 73	70'7 69'1 67'4 65'7	0.6 0.6 0.6	0.421 0.410 0.634	*013 *012 *011 *011	8.0 7.5 7.1 6.7	0'1 0'1 0'2	4.4 4.9 5.3 5.7	0.2	64 60 57 54	3 3	490.8 491.1 3 .5 491.8	1100	*01 0.2 *02 0.3 *03 0.5 *04 0.7
	72 71 70 69 68	64.1 62.4 60.8 59.1 57.4	0.6 0.6 0.6	0'598 0'564 0'532 0'501	.000 .008 .007	6·3 6·0 5·6 5·3	-0.1 0.1 0.1 0.1 0.1	6·1 6·4 6·8 7·1 7·4	0.2	51 48 45 43 41	3 2 2 2	492.0 *2 *4 *6 492.8		'05 0'9 '06 1'0 '07 1'2 '08 1'4 '09 1'5

of T	ding her- eter.	Temperature of the Dew-Point.	Difference for an increase of 1° in Dry.	Elastic force of Vapour.	Difference for an in- crease of 1° in Dry.	Vapour in a Cubic Foot of Air.	Difference for an in- crease of 1° in Dry.	Vap. reqd. to sat. a Cubic Foot of Air.	Difference for an in- crease of 1º in Dry.	Degree of Humidity. (Satn. = 100.)	Difference for an in-	Weight of a Cubic Foot of Air. Bar. reading 29 inches.	Diff. for an increase of 10 in Dry	Difference for one inch in Barometer and proportional parts.
84	68 67 66 65 64 63 62	57'4 55'8 54'1 52'5 50'8 49'1 47'5	-0.6 0.6 0.6 0.6 0.6 0.5	in. 0'472 0'445 0'419 0'394 0'371 0'349 0'328	in. '006 '006 '006 '006 '006 '006	gr. 5'0 4'7 4'5 4'2 4'0 3'7 3'5	0,1 0,1 0,1 0,1 0,1 0,1 e.1	gr. 7'4 7'7 7'9 8'2 8'4 8'7 8'9	gr. +0'5 0'5 0'5 0'5 0'5 0'5	41 38 36 34 32 30 28	- 2 2 2 2 2 2 2 1	grs. 492.8 492.9 493.1 -2 -4 -5	+16.8 - 0.8 - 8	16·8 in. grs. '1 1·7 '2 3·4 '3 5·0 '4 6·7 '5 8·4 '6 10·1
85	85 84 83 82 81 80 79 78	45.8 85.0 83.4 81.7 80.0 78.4 76.7 75.1 73.4	-0.5 -0.6 0.6 0.6 0.6 0.6 0.6 0.6	0°308 1°1203 1°141 1°082 1°026 0°973 0°922 0°873 0°826	'006 '023 '021 '020 '018 '018 '018 '018 '018	3'3 12'8 12'1 11'5 10'9 10'3 9'7 9'7 9'8	-0'1 -0'3 0'3 0'3 0'2 0'2 0'2 0'2	9°1 0°0 0°7 1°3 1°9 2°5 3°1 3°6 4°1	+0°5 +0°7 0°7 0°7 0°6 0°6 0°6 0°6	26 100 95 90 85 80 76 72 68	- 1 - 5 5 5 4 4 4 4 3	493.8 487.4 487.8 488.2 .5 488.8 489.2 .5 489.8	+ 16.8	'6 10'1 '7 11'8 '8 13'4 '9 15'1
	77 76 75 74 73 72 71 70 69	71.8 70.1 68.5 66.8 65.2 63.5 61.8 60.2 58.5	0.6 0.6 0.6 0.6 0.6 0.6	0.781 0.738 0.698 0.660 0.623 0.588 0.555 0.524	*018 *017 *017 *017 *016 *015 *014 *014 *014	8·3 7·8 7·4 7·0 6·6 6·2 5·9 5·5 5·2	0°2 0°2 0°2 0°2 0°2 0°2 0°1 0°1	4.5 5.0 5.4 5.8 6.2 6.6 6.9 7.3 7.6	0.6 0.6 0.6 0.6 0.6 0.6 0.6 0.5	64 61 58 55 52 49 46 43 40	3 3 3 3 3 2 2 2 2	490°0 -3 -6 490°8 491°0 -2 -4 -6 491°8		
86	68 67 66 65 64 63 62 86	56.9 55.2 53.6 51.9 50.2 48.6 46.9	0.6 0.6 0.5 0.5 0.5 -0.5	0'466 0'439 0'413 0'388 0'365 0'343 0'322	'013 '012 '011 '009 '008 '007 -'006	4'9 4'6 4'3 4'1 3'8 3'6 3'4	-0.3 -0.1 0.1 0.1 0.1 0.1 0.1	7'9 8'2 8'5 8'7 9'0 9'2 9'4	+0.2 +0.2 +0.2 +0.2 +0.2	38 36 34 32 30 28 27	2 2 2 1 1 1 - 1	492°0 °2 °3 °6 °8 492°9 486°2	- o·8	
	85 84 83 82 81 80 79 78 77	84.3 82.7 81.1 79.4 77.8 76.1 74.5 72.8 71.2	0.6 0.6 0.6 0.6 0.6 0.6	1'180 1'121 1'064 1'008 0'955 0'904 0'855 0'808 0'763	'023 '023 '022 '022 '021 '020 '018 '016 '014	12.5 11.8 11.5 9.5 9.0 8.5 9.0 8.5	0'3 0'2 0'2 0'2 0'2 0'2 0'2 0'2	0.7 1.4 2.0 2.6 3.1 3.7 4.2 4.7 5.1	0.7 0.6 0.6 0.6 0.6 0.6 0.6	95 90 85 80 76 72 68 64 61	5 5 4 4 4 4 4 3 3 3	486.6 487.0 487.7 488.1 488.7 489.0		
	76 75 74 73 72 71 70 69 68 67	69.5 67.9 66.2 64.6 62.9 61.3 59.6 58.0 56.3	0.6	0.721 0.681 0.643 0.607 0.573 0.510 0.480 0.452 0.426	.008	7.6 7.2 6.8 6.4 6.1 5.7 5.4 5.1 4.8 4.5	0'2 0'2 0'2 0'1 0'1 0'1 0'1	5.6 6.0 6.4 6.8 7.1 7.5 7.8 8.1 8.4 8.4	0;6 0:6 0:6 0:5 0:5 0:5 0:5	58 55 52 49 46 43 40 38 36 34	3 3 2 2 2 2 2 2 2 2 2 2	489°7 490°0 *2 *4 *6 490°8 491°0 *1		
87	66 65 64 63 87 86 85 84	53.0 51.4 49.7 48.1 87.0 85.4 83.7 82.1 80.4	0.5 0.5 -0.5 -0.6 0.6 0.6	0'402 0'379 0'357 0'336 1'282 1'219 1'158 1'098	'007 '006 '006 -'006 -'024 '024 '024	4.2 4.0 3.7 3.5 13.6 12.9 12.2 11.6 11.0	0.1 0.3 0.3 0.3 0.3 0.1 -0.1	9.0 9.2 9.5 9.7 0.0 0.7 1.4 2.0 2.6	+0.2 +0.2 +0.2 0.3 0.4 0.4 0.4 0.7 0.7 0.7 0.7 0.7 0.7 0.7 0.7	32 30 28 27 100 95 90 85 81	5	485.2 485.6 486.0	+16·7	'01 0'2 '02 0'3 '03 0'5 '04 0'7 '05 0'8 '06 1'0 '07 1'2 '08 1'3 '09 1'5

of 7	ding Ther- neter.	Temperature of the Dew-point,	Difference for an in- crease of 1° in Dry.	Elastic force of Vapour.	Difference for an increase of 10 in Dry.	Vapour in a Cubic Foot of Air.	Difference for an in- crease of 1° in Dry.	Vap. reqd. to sat. a Cubic Foot of Air.	Difference for an in- crease of 1° in Dry.	Degree of Humidity. (Satn.=100.)	Difference for an in- crease of 1° in Dry.	Weight of a Cubic Foot of Air. Bar. reading 29 inches.	Diff. for an increase of 10 in Dry	Difference for one	and proportional parts.
Dry.	Wet.	50	9 8	NE VE	9 9	E V	A 2	20	99	D:8	9 9	27.5	of Di	E.A	and
87	83 82 81	80.4 78.8 77.1	0.6	in. 1'040 0'985 0'933	in. '022 '021 '020	gr. 11'0 10'4 9'8	gr. -0°2 0°2 0°2	3.5 3.5 3.8	+0.6 0.6 0.6	81 77 73	- 4 4 4	487'1	+16.4 - 0.8	-	r7 grs.
	80 79 78	75.5 73.9 72.2 70.6	0.6	0.884 0.837 0.792	*019 *018 *016	8.3 8.8 8.8	0°2 0°2 0°2	4·3 4·8 5·3 5·7	0.6	69 65 61 58	4 4 3	487.7 488.0 -2		·2 ·3 ·4	3'3 5'c 6'7
	77 76 75 74	68·9 65·6	0.6	0.749 0.669 0.632	*015 *014 *013	7.9 7.4 7.0 6.6	0.1 0.1 0.1	6.6	0.2	55 52 49	3 3 3 3	200		7 1	8.4
	73 72 71	64 0 62.4 60.7	0.6	o*597 o*564 o*532	'012 '010	5.6 2.9		7°3 7°7 8°0	0.2	46 43 41	2 2 2	489.8			15'0
	70 69 68 67	59°1 57°4 55°8 54°1	0.2	0°502 0°473 0°446 0°420	.000 .000 .000	5°3 5°0 4°7 4°4	0,1 0,1 0,1	8.3 8.6 8.3	0.2	39 37 35 33	2 2 2	490.0			
	66 65 64	52.5 50.8 49.2	0.2	0°395 0°372 0°351	*008 *007 —*006	4°2 3°9 3°7	-0,1 0,1 0,1	9°4 9°7 9°9	+0.2	31 29 27	2 1 - 1	·7 ·8 490·9		4	
88	88 87 86	88°0 86°4 84°7	0.6 0.6	1.323 1.323	- '024 '023 '023	14.0	-0.3 -0.3	0°0 0°7 1°4	+0.7	100 95 90	- 5 5 5	484.0 .4 484.8	- 0.8		
	85 84 83	81.2 83.1	0.6 0.6	1.134 1.018	'022 '021 '020	11'4	0.3	2.0	0.7	85 81 77	4 4	485'9	7107		
	82 81 80	78°2 76°5 74°9	0.6	0.865 0.862	,018 ,018 ,010	9.6 9.1 8.6	0°2 0°2	3·8 4·4 4·9	0.6	73 69 65 61	4 3 3	486.3			
	79 78 77 76	73°3 71°6 70°0 68°4	0.6	0'775 0'733 0'693	*018 *017 .016	8·1 7·7 7·3	0°2 0°2 0°2	5°4 5°9 6°3 6°7	0.6	58 55 52	3 3 3	487.2 *4 *7 487.9			
	75 74 73	65°1 63°4	0.6	0.282	.013 .013	6.2	0,1 0,1	7°1 7°5 7°9	0.2	49 46 43	3 2 2	488.2			
	72 71 70 69	61.8 60.2 58.5 56.9	0.2	0.553 0.522 0.464	*012 *011 *010 *009	5°8 5°5 5°2 4°9	0,1 0,1 0,1 0,1	8·5 8·8 9·1	0.2	39 37	2 2	488.8			
	68 67 66	22.0 23.6 22.5	0.2	0.437	*008 *007 *006	4.6 4.3 4.1	0,1 0,1 0,1	9°4 9°7 9°9	0.2	35 33 31 29	2 1 1	·6 ·6			
89	65 89 88	50'3 89'0 87'4	-0.6 0.6	0.362	- '006 - '024	3.8	-0.3	0.0	+0.2	100	- 1 - 5	482.9	- 0.8		-
	87 86 85	85.7 84.1 82.2	0.6	1'299 1'172 1'172	*023 *022 *021 *020	13.4 13.0 13.0	0.3	0°7 1°4 2°1 2°7	0.4	95 90 85 81	5	483°3 483°7 484°1	+16.7		
	84 83 82	79°2 77°6	0.6	0.998	.019 .014	10,0	0°2 0°3	3°3 3°9 4°4	0.6	77 73 69	4	484.8	190		
	81 80 79 78	76.0 74.3 72.7 71.1	0.6	0.895 0.847 0.801 0.757	'015 '014 '013 '012	9'4 8'9 8'4 8'0	0°2 0°2 0°2	5°0 5°5 6°0 6°4	0.6	65 61 58	3 3	485·8 486·1		'02 0	0'2
	77 76 75	69'4 67'8 66'2	0.6	0.640	'012 '012 '011	7.2	0,1 0,1	6·9 7·3 7·7	0.2	55 52 49 46	2 2	486·9 487·1		·04 0	7 8
	74 73 72	64.6	0.6	0.602	010, 010,	6.4 6.0 5.7	-0.1 0.1 0.1	8.0	+0.2	43 41 39	2 2	187.9		'07 I	.1

Readi of The mome	er-	Temperature of the Dew-Point.	Difference for an in- crease of 1° in Dry.	Elastic force of Vapour.	Difference for an ir- crease of 1° in Dry.	Vapour in a Cubic Foot of Air.	Difference for an in- crease of 1° in Dry.	Vap. read. to sat. a Cubic Foot of Air.	Difference for an in- crease of 1° in Dry.	Degree of Rumi- dity. (Satn.=100.)	Difference for an in- crease of 1° in Dry.	Weight of a Cubic Foot of Air. Bar. reading 29 inches.	Diff. for an increase of 1 in . in Bar.	Difference for one inch in Barometer and proportional purts.
Dry. V	Vet.	Tem	Diff	Vap	Diff	Vap	Diffe	Vap	Diff	Deg	Diffe	Wei Fool	of 1	Differ inch i and parts.
	72 71 70 69 68 67 66	61°3 59°6 58°0 56°4 54°7 53°1 51°5	-0.2 0.2 0.2 0.2 0.2 0.2 0.2	in. 0'541 0'511 0'482 0'455 0'429 0'404 0'381	in '010 '010 '009 '009 '008 '007 - '006	gr. 5.7 5.4 5.1 4.8 4.5 4.2 4.0	-0.1 0.1 0.1 0.1 0.1 0.1 0.1 d.1	gr. 8.7 9.0 9.3 9.6 9.9 10.2	gr. +0'5 0'5 0'5 0'5 0'5 +0'5	39 37 35 33 31 29 28	- 2 2 2 2 1 1	grs. 487'9 488'1 '3 '4 '6 '8 488'9	+ 16.7	16·6 in. grs. '1 1'7 '2 3'3 '3 5'0 '4 6·6 '5 8'3 '6 10'0
	90 89 88 87 86 85 84 83 82 81 80 77 76 75 74 73 72 71 70 68 67	90°0 88°4 86°8 85°1 83°5 80°3 78°6 77°0 75°4 73°7 72°1 70°5 68°8 67°2 65°6 64°0 62°4 60°7 59°1 57°5 55°8 54°2 52°6	-0.6 0.6 0.6 0.6 0.6 0.6 0.6 0.6 0.5 0.5 0.5 0.5 0.5 0.5 0.5 0.5 0.5 0.5	1'411 1'342 1'276 1'212 1'151 1'092 1'036 0'982 0'930 0'880 0'745 0'745 0'665 0'629 0'595 0'562 0'531 0'501 0'473 0'446 0'421 0'397	'027 '026 '026 '025 '024 '023 '022 '021 '020 '018 '017 '016 '015 '014 '013 '013 '013 '012 '010 '009 '008 '007	14.8 14.1 13.4 12.7 12.1 11.4 10.8 10.3 9.7 9.2 8.7 8.3 7.8 7.4 7.0 6.6 6.2 5.9 5.6 5.3 5.0 4.7 4.4 4.2	-0'3 0'3 0'3 0'3 0'3 0'3 0'2 0'2 0'2 0'2 0'2 0'2 0'2 0'1 0'1 0'1 0'1 0'1 0'1 -0'1	0°0 0°7 1°4 2°1 2°7 3°4 4°5 5°6 6°1 6°5 7°4 7°8 8°2 8°9 9°2 9°5 9°8 10°1 10°6	+0.8 0.8 0.8 0.7 0.7 0.7 0.7 0.7 0.7 0.7 0.7 0.7 0.6 0.6 0.6 0.6 0.6 0.6 0.6 0.6 0.6 0.6	95 95 85 87 77 73 69 65 65 56 53 50 47 44 42 40 38 36 34 32 32 32 8	- 5544444333333334444A4333333344444444444	481'8 482'3 482'7 483'1 483'8 484'1 484'8 485'1 466 486'8 487'0 2 47'5 77'487'8 488'0	+16.6	'6 10'0 '7 11'6 '8 13'3 '9 14'9
91	91 90 89 88 87 86 85 84 83 82 81 80 79 76 75 74 73 72 71 70 69	91°0 89°4 87'8 86°1 84°5 82°9 81°3 79°7 78°0 76°4 74'8 73°2 71°6 69'9 68°3 66°1 63°5 66°2 58°6 57°0 55°3 53°7	-0.6 0.6 0.6 0.6 0.6 0.6 0.6 0.6 0.6 0.6	1'455 1'384 1'316 1'250 1'187 1'127 1'069 1'013 0'960 0'862 0'772 0'730 0'652 0'652 0'652 0'550 0'550 0'463 0'443	- '027 '027 '027 '026 '025 '023 '021 '019 '017 '016 '015 '014 '013 '011 '010 '009 '009 '009 '009 '009 '009	15'3 14'5 13'8 13'1 12'5 11'8 11'2 10'6 10'1 9'5 9'0 8'5 8'1 7'7 7'2 6'8 6'5 6'1 5'8 5'5 5'5 5'5 14'8 4'5 4'3	-0.3 0.3 0.3 0.3 0.3 0.3 0.3 0.2 0.2 0.2 0.2 0.2 0.1 0.1 0.1 0.1 0.1 0.1 0.1 0.1 0.1 0.1	0°0 0°8 1°5 2°2 2°8 3°5 4°1 4°7 5°2 5°8 6°3 6°8 7°2 7°6 8°1 8°5 8°8 9°2 9°5 9°8 10°5 10°8 11°0	+0.7 0.7 0.7 0.7 0.6 0.6 0.6 0.6 0.6 0.6 0.6 0.5 0.5 0.5 0.5 0.5 0.5 0.5 0.5 0.5 0.5	95 90 86 82 78 74 70 66 62 59 56 53 50 47 44 42 40 38 36 34 32 30 28	5 4 4 4 4 4 4 4 3 3 3 3 3 3 3 3 2 2 2 2 2	481.1 5 481.9 482.3 482.6 483.7 484.0 3 5 484.8 485.1 3 5 485.8 486.0 11 3 5 486.8 487.0	+16.6	'01 0'2 '02 0'3 '03 0'5
92	92 91 90 89 88 87	92'0 90'4 88'8 87'1 85'5 83'9	-0.6 0.6 0.6 0.6 -0.6	1'501 1'428 1'357 1'289 1'224 1'162	-*028 *027 *025 *024 *023 -*022	15'7 14'9 14'2 13'5 12'8	-0.3 0.3 0.3 0.3 0.3	0.0 0.8 1.5 2.2 2.9 3.5	+0.8 0.8 0.8 0.8 0.8 0.8	95 90 85 81 77	5 4 4 4	479°5 480°0 °4 480°8 481°2 481°5	+16.6	'04 0'7 '05 0'8 '06 1'0 '07 1'2 '08 1'3 '09 1'5

of	eading Ther- ometer.	Temperature of the Dew-Point,	Difference for an in- crease of 10 in Dry.	Elastic force of Vapour.	Difference for an in- crease of 10 in Dry.	Vapour in a Cubic Foot of Air.	Difference for an in- crease of 1° in Dry.	Vap, read, to sat, a	Difference for an in-	Degree of Humi-	Difference for an in-	Weight of a Cubic Foot of Air. Bar.	Diff. for an increase of 15 in Dry	Difference for one inch in Barometer and pare.
92	87 86 85 84 83 82 81 80 79 78 77 76 75 74 73 72 71	83'9 82'3 80'7 79'1 77'5 75'9 74'2 72'6 71'0 69'4 67'8 66'2 64'5 62'9 61'3 59'7 58'1 56'5 54'8	0.6 0.6 0.6 0.6 0.6 0.5	in. 1'162 1'103 1'047 0'994 0'943 0'894 0'802 0'759 0'718 0'679 0'642 0'667 0'573 0'541 0'483 0'456 0'430	in '022 '020 '020 '020 '019 '018 '017 '015 '014 '013 '011 '009 '008 '008 '007 - '007	11.6 11.6 9.9 9.3 8.8 8.8	0'3 0'3 0'2 0'2 0'2 0'2	gr. 3'5 4'1 4'7 5'3 5'8 6'4 6'9 7'4 7'8 8'2 8'2 8'6 9'0 9'4 9'7 10'0 10'4 10'7 10'9 11'2	0.3 0.8 0.7 0.7 0.7 0.7 0.7	777 737 766 662 599 566 533 500 477 453 431 338 341 322 302 28	4 3 3 3 3 3 3 2 2 2 2 2 2 2 2 1	481.9	grs 0.3	in. grs.
93	93 92 91 90 89 88 87 86 85 84 83 82 81 80 79 78 77 76 75 74 73 72 71	93°0 91'4 89'8 88'2 86'6 85'0 83'4 80'1 78'5 76'9 75'3 73'7 72'1 70'5 68'9 67'2 65'6 64'0 62'4 60'8 59'2 57'6 56'0	-0.6 0.6 0.6 0.6 0.6 0.6 0.5 0.5 0.5 0.5 0.5 0.5 0.5 0.5 0.5 0.5	1'548 1'473 1'401 1'332 1'266 1'203 1'142 1'084 1'028 0'974 0'923 0'874 0'704 0'666 0'630 0'596 0'564 0'533 0'503 0'475 0'449	-'028 '027 '026 '025 '024 '022 '021 '020 '018 '016 '015 '014 '013 '012 '011 '010 .009 '009 '009 -008	16'2 15'4 14'7 14'0 13'3 12'6 11'9 11'3 10'7 10'2 9'6 9'1 8'7 8'2 7'8 7'4 6'6 6'6 6'2 5'9 5'5 5'5 5'5 5'5 4'7	-0'3 0'3 0'3 0'3 0'3 0'3 0'2 0'2 0'2 0'2 0'2 0'2 0'1 0'1 0'1 0'1 0'1 0'1 0'1 0'1	0°0 0°8 1°5 2°2 2°9 3°6 4°3 4°9 5°5 6°6 6°6 7°1 7°5 8°4 8°8 9°3 9°6 10°0 10°3 10°7 11°2 11°2	+0.8 0.8 0.8 0.7 0.7 0.7 0.7 0.7 0.7 0.7 0.7 0.7 0.7	95 90 86 82 78 74 70 66 63 60 57 54 51 48 45 42 40 38 36 34 32 30 29	5 4 4 4 4 4 4 4 4 4 4 4 4 4 4 4 4 4 4 4	478.4 478.9 479.3 479.7 480.1 5 480.9 481.9 481.9 482.2 5 482.8 483.0 3 5 483.7 484.0 2 4 5 84.0 2 4 88.0 3 88.0 18.0	+16.2	
94	94 93 92 91 90 89 88 87 86 85 84 83 82 81 80 79 78	94°0 92°4 90°8 89°2 87°6 86°0 84°4 82°8 81°2 79°6 78°0 76°4 74°8 73°1 71°5 69°9 68°3 66°7 65°1	-0'6 0'6 0'6 0'6 0'6 0'6 0'6 0'6 0'6 0'6	1'520 1'446 1'375 1'307 1'242 1'180 1'121 1'064 1'010 0'958 0'909 0'862 0'816 0'772 0'731 0'692 0'655	*025 *024 *023 *022 *022 *021 *020	16·7 15·9 15·1 14·4 13·7 13·0 12·3 11·7 11·1 10·5 10·0 9·5 9·0 8·5 8·0 7·6 7·2 6·8 6·4	-0.3 0.3 0.3 0.3 0.3 0.3 0.3 0.3	0°0 0°8 1°6 2°3 3°7 4°4 5°0 5°6 6°2 6°7 7°2 7°7 8°2 8°7 9°5 9°9 10°3	+0.8 0.8 0.8 0.8 0.7 0.7 0.7 0.7 0.7 0.7 0.7 0.7	95 90 86 82 78 74 70 66 63 60 57 54 51 48 45 43 41 39	5 4 4 4 4 4 4 4 4 4 4 4 4 4 4 4 4 4 4 4	77'2 77'7 78'1 78'6 79'7 80'1 50'8 81'7 82'0 22 57 32'9 83'1	- 0·8 + 16·5	*01 0'2 '02 0'3 '03 0'5 '04 0'7 '05 0'8 '06 1'0 '07 1'2 '08 1'3 '09 1'5

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1		Temperature of the Dew-Point.	Difference for an in- crease of 1° in Dry.	Jo	Difference for an in- crease of 1° in Dry.	Cubic	Difference for an in- crease of 1° in Dry.	Vap. reqd. to sat. a Cubic Foot of Air.	Difference for an in crease of 1° in Dry.	Humi-	Difference for an in crease of 1° in Dry.	ubic Bar.	Diff. for an increase of 10 in Dry	one	Tel I
	her-	re o	in for	force	for	The same	in in	to	E H		Difference for an in crease of 1° in Dry.	0 0	inc.	for	proportional
1000000	acter.	ratu	nce of 1	1000	of 1	r in a	of 10	Foot	nce of 1	Satn.	oce l	of a Air. 29 in	for an ince 10 in Dry in, in Bar.	Bar	ropo
		w-P	Tere	Elastic Vapour.	lere 386	Vapour Foot of	Difference for crease of 1° in	Die r	lere ase	Degree dity. (Si	Ferrer 1	Weight Foot of reading	lo lo	in	D.
Dry.	Wet.	Ten	Did or	Ela	Dif	Va	Dif	Car	Dif	Deg	Diff	We Foo	Diff.	Difference for one	and parts.
	0	. 0	0	in.	in.	gr.	gr.	gr.	gr.			grs.	grs.		
94	76	65.1	-0.2	0.620	-,010	6.1	-0,1	10.9	+0.6	39	- 2	483.1	- 0.8	16	5.4
	75 74	63.5	0.2	0.222	,010	5.7	0,1	11.0	0.6	37	2 2	*3	+16.2	in.	grs.
1	73	60.3	0.2	0.24	.010	5.4	0,1	11.3	0.6	33	1	.7	+105	'I	1.6
	72	58.7	0.2	0'494	.009	2,1	0,1	11.6	0.6	31	1	483.9	150	.3	4'9
	71	57.1	-0.2	0.466	008	4'9	-0.1	11.8	+0.6	29	- 1	484.0		4	6.6
95	95	95'0	-0.6	1.646	-1030	17'2	-0.3	0.0	+0.8	100	- 5	476.2	- 0.8	.6	9.8
	94	93.4	0.6	1.267	1029	16.3	0.3	0.9	0.8	95	5	476.6	+16.4		11.2
	92	90'2	0.6	1'420	*027	14.8	0.3	2.4	0.8	86	4	+//-5	7104		13.1
	91	88.6	0.6	1'350	'026	14.1	0.3	3.1	0.8	82	4	477'9	-	3	
	90	87.0	0.2	1'283	'024	13.4	0.3	3.8	0.8	78 74	4	478.3	37. 9		
	88	83.8	0.2	1.128	1020	12.1	0.3	2.1	0.8	70	4	479'1	Post I	-	
	87	82'2	0.2	1.099	,018	11.2	0.3	5'7	0.8	66	3	.5	1300	-	15 15
	86	80.6	0.2	0.990	'017	10,3	0.5	6.3	0'7	63	3	479'8			
	84	77'4	0.2	0'940	.016	9.8	0.5	7.4	0.4	57	3	4.00		100	
	83	75.8	0.2	0'892	,019	9'3	0'2	7'9	0'7	54	2	480.7			
	82	74.2	0.2	0.846	*015 *014	8.8	0'2	8.4	0'7	51 48	2 2	481.0	1000		77
	80	71.0	0.2	0.759	*013	7.9	0.5	9.3	0.7	45	2	.3			
	79	69.4	0.2	0'718	'012	7'5	0'2	9.7	0.4	43	2	481.7			
-	78	67.8	0.2	0.680	'012	7'1	0'2	10,2	0.4	41	2	482'0	1		
	77 76	64.6	0.2	0,610	,010	6.3	0°2	10.0	0.4	39 37	2	·4	200		
	75	63'0	0.4	0.577	.009	6.0	0.1	11'2	0.6	35	2	.6	198.1		
	74	61.4	0.4	0.545	.008	5.6	0.1	11.6	0.6	33	2	482.8	37.1		3
	73	59.8	-0.4	0'514	-'007	5'3	0.1	11.0	+0.6	31	- 1	483.0	1000		1
	100								111111111111111111111111111111111111111	13.0	199	200			. :
96	96	96.0	-0.6	1.616	-,030	16.8	-0.3	0.0	+0.8	95	- 5	475'0	0.8		
	95	92.8	0.6	1,238	*028	16.0	0.3	1.7	0.8	90	4	475'9	+16.4		1
	93	91'2	0.6	1.464	*027	15'2	0.3	2.2	0.8	86	4	476.4	Print		- 1
	92	88.0	0.6	1,352	025	14.2	0.3	3.5	0.8	78		476.8			1
	91	86.4	0.6	1,500	*022	13,1	0,3	4.6	0.8	74	3	477.6			
	89	84'9	0.6	1,108	'021	12'4	0'2	5.3	0'7	70	3	478.0			
	88 87	83.3	0.6	1,138	*020 *019	11.8	0'2	6·5	0.7	66	3	478.7			
	86	81.4	0.6	1.059	*017	10'7	0'2	7.0	0.7	60		4790	-		
	85	78.5	0.2	0'974	.016	10.1	0'2	7.6	0'7	57	3	*3	1		,
	84	76.9	0.2	0.876	'015	9.1	0'2	8.9	0.7	54	3	·6 479'9	-		- 1
	83	75'3	0.2	0.831	014	8.6	0'2	9.1	0'7	49	2	480.5	100		75.4
	81	72'1	0.2	0.488	.013	8.5	0'2	9.2	0'7	46	2	. '5	1 11		
	80	70'5	0.2	0'746	'012	7.7	0,1	10.0	0.6	43	2	480.9			
	79 78	68.9	0.2	0.668	,010	6.9	0,1	10.8	0.6	39	2	481'2	WHI I		
	77	65.7	0.2	0.633	,010	6.5	0,1	11'2	0.6	37	2	.4	177		- 1
	76	64'2	0.2	0.600	.010	6.5	0,1	11.8	0.6	35	2	.8			-
	75 74	61.0	0.2	0.268	,010	2.6 2.9	0,1	12.1	0.6	31	1	481.9			400
	73	59'4	-0.4	0.207	008	5'3	-0.1	12.4	+0.6	30	- 1	482.1		'01	0.3
97	97	97.0	-0.6	1.750	030	18'2	-0'3	0.0	+0.8	100		473.8	- 0'7	.03	0.2
	96	954	0.6	1.666	'027	17'3	0.3	0.0	0.8	95	5	474'3	1.6.	.04	0.2
	95	93.8	0.6	1.286	025	16.2	0.3	2.2	0.8	86	4	474.7	+16.4	.06	1,0
	94 93	90.6	0.6	1'510	*024	15.7	0,3	3.3	0.8	82	4	475.6	100	.07	1'2
9 14	92	80.1	0.6	1.368	.023	14'2	0'3	4.0	0.8	78	4	476.1		.03	1.3
	91	87.5	-0.6	1,305	022	13.2	-0.3	4.7	+0.8	74	3	476.5		91	1.2
					-	-		-		-		NAME OF TAXABLE PARTY.	-		

ſ			e e	n in-	1 2	n in-	Cubic	an in-	at. a	n in-	in 00	Day.	ubic 3ar.	rease	one	eter
	of T	ding her-	Temperature of the Dew-Point.	Difference for an in- crease of 1° in Dry.	force	Difference for an in- crease of 1° in Dry.			Vap. regd. to sat.	Difference for an in- crease of 1° in Dry.	Degree of Humi- dity. (Satn.=100.)	Difference for an in- crease of 1° in Dry.	Weight of a Cubic Foot of Air. Bar. reading 29 inches.	Diff. for an increase of 10 in Dry	Difference for	meh in Barometer and proportional parts.
	mon	neter.	opera v-Pop	erenc use of	Elastic Vapour.	erenc use of	Vapour in a Foot of Air.	Difference for crease of 1° in	require Fo	ference use of	rree (Sa	ference	ight of h	f. for	erene	is in
1	Dry.	Wet.	Ten	Diff	Ela Veg	Diff	Vap	Diff	Cal	Diff	Des	Diff	Foc reac	Diff	Diff	and parts.
	97	91	87.5	-0.6	in. 1°302	in. 022	gr. 13'5	gr. -0'3	gr. 4'7	+0.8	74	- 3	grs. 476'5	grs. - 0°7	1	6.3
1		90	85'9	0.6	1.172	'02 I	12.8	0.5	5'4	0.4	67	3	476.8	+16.4	in.	grs.
-		88	82.7	0.2	1.118	.019	11.6	0'2	6.6	0.4	64	3	.6	-	1.2	3.3
1		87 86	79.5	0.2	1.000	.010	11'0	0.5	7.8	0.4	57	3	477'9		.4	6.5
1		85	78.0	0.2	0.909	.018	9'9	0'2	8.8	0'7	54 52	3	478.8		.5	8.2
1		83	74'8	0.2	0.863	.015	8.9	0'2	9.8	0.7	49	2	479'1		1 .7	11'4
		82	73'2	0.2	0.775	.014	8.4	0'2	10'2	0.4	46 44	2	.4		.8	13'0
		80	70'0	0.2	0.695	'012	7.6	0.1	11.0	0.4	42 39	2 2	479°9		-	
		79 78	66.8	0.2	0.658	'010	6.8	0.1	11'4	0.6	37	2	*3		100	
-		77 76	65.3	0.2	0.623	,010	6.1	0,1	11.8	0.6	35 33	1	.5		1	
		75	60.2	0.4	0.228	-,008	5.8	-0.1 0.1	12'4	+0.6	31	- 1	480.9			
1	8	98	98.0	-0.6	1.807	-1032	18.7	-0.3	0.0	+0.0	100		472.7	- 0.7	1	
1		97	96.4	0.6	1.639	.031	17.8	0.3	0.0	0.0	95	4	473'2	+16.3		
		96	93'3	0.6	1.261	'029	16.5	0.3	1.7	0.9	90 86	4	473'7 474'2	T10 3		
1		94	90.1	0.6	1.487	*025 *023	15.4	0,3	3'3	0.0	82 78		474.6			
1		92	88.5	0.2	1.347	'021	13'9	0,3	4.8	0.0	74	3	. 4			
1		91	85.3	0.2	1'218	'019	13.5	0.3	2.2	0.0	67	3	475.8	12.16		
		89	83.8	0.2	1.124	.012	11'4	0.3	6.7	0.8	64	3	476.9		1	
1		87	80.6	0.2	1'043	'014	10.8	0'2	7.9	0.8	58	3	477.3		1	
		85	79'0	0.2	0'990	,013	9'7	0'2	8.5	0.8	55 52	3 2	The second second			
		84 83	75'9	0.2	0.893	'013	9°2 8°7	0'2	9.2	0.8	49 46	2	477'9 478'2 '4			
1		82	72.7	0.2	0.804	'012	8.3	0'2	10.4	0.8	44	2	.7			
		80	99.5	0.2	0.762	.010	7.8	0,1	11,3	0.4	42		478°9			
-		79 78	66.4	0.2	0.684	1009	7°1	0,1	11.6	0.4	38 36	2 2	.4			
1		77	64.8	0.2	0.613	.008	6.3	0,1	12.4	0.4	34	2	479'8			
-	1	76 75	63.5	-0.4	0.280	008	6·0 5·7	-0.1 0.1	13.0	+0.4	32		180.0			
9	19	99		-0.6	1.862	- '034	19.3	-0.4	0.0	+0.9	100		171'5	- 0.4		-
	1	98	97'4	0.6	1.690	'030	17.5	0'4	0.9	0.0	951	5 4	172'0	+16.3		1
1	-	96 95	94'3	0.6	1.234	'029 '028	16.7	0'4	2.6	0.9	87	4 4	73'0			1
-	-	94	91.1	0.6	1.462	'027	12.1	0,3	4'2	0.8	8 ₃	4 4	·5 -73'9			- 1
1	-	93	88.0	0.6	1,352	*026 *026	14.4	0.3	4°9 5°6	0.8	7.5 7.1		74°3			
-		91	86.4	0.2	1.563	'025	13.0	0.3	6.3	0.8	67	3 4	75"1			
1		89	83'2	0.2	1'141	*025	11.7	0'2	7.6	0.4	64	3 4	75'9	-		-
-		87	80.1	0.2	1.034	*024	10.2	0,1	8.8	0.4	58	3 4	76.5		'01	0.3
		86 85	78.5	0.2	0'977	1022	9.5	0.1	9.8	0.6	52	2 4	76.8		.03	0.2
		84 83	75'4	0.2	0.880	,019	0.0	0.1	10.3	0.6	49	2	77'1		.04	0.8
-	-	82	73.8	0.2	0.832	'017	8.1	0.1	10'7	0.6	44 42	2 4	·6 -77'9		·06	1.0
-		80	70.6	-0.2	0'751	-014	7.7	-0.1 0.1	11.6	+0.6	40	2 4	78.1	1	*08	T'3
_	- 1.				!	_ 1					3	1	704		*09	1.2

-		11 41	100		- 1		1							
of mor	ading Ther- neter.	Temperature of the Dew-point.	Difference for an in- crease of 1° in Dry.	Elastic force of Vapour,	Difference for an in- crease of 1 in Dry.	Vapour in a Cubic Foot of Air.	Difference for an in- crease of 19 in Dry.	Vap. reqd. to sat. a Cubic Foot of Air.	Difference for an in- crease of 1° in Dry.	Degree of Humidity. (Satn. = 100.)	Difference for an in- crease of 1° in Dry.	Weight of a Cubic Foot of Air. Bar. reading 29 inches.	Diff. for an increase of 1 in. in Bar.	Difference for one inch in Barometer and proportional parts.
Dry.	Wet.	89	G 9	- E	O 9	N. B.	99	20	8	Q.B	ig a	Fo Fo	of Di	Differ inch and parts.
99	80 79 78 77 76	69.1 67.5 65.9 64.3 62.8	-0.5 0.4 0.4 -0.4	in. 0.712 0.675 0.639 0.605 0.572	in'013 '011 '011 -'010	gr. 7'3 6'9 6'6 6'2 5'9	-0.1 0.1 0.1 0.1 e.1 dr.	gr. 12'0 12'4 12'7 13'1 13'4	+0.6 0.6 0.6 0.6 dr.	38 36 34 32 31	- 2 2 2 1 - 1	grs. 478'4 '6 478'8 479'0 479'2	+16.3	16'2 in. grs. 'I 1'6 '2 3'2 '3 4'9
100	99 98 97 96 95 94 93 92 91 90 89 88 87 86 85	98'4 96'9 95'3 93'7 92'1 90'6 89'0 87'4 85'9 84'3 82'7 81'2 79'6 78'0 76'5	-0.6 0.6 0.6 0.6 0.6 0.6 0.6 0.5 0.5 0.5 0.5	1'918 1'828 1'742 1'660 1'582 1'508 1'437 1'368 1'301 1'237 1'175 1'116 1'060 1'066 0'955	- '035 '033 '031 '029 '027 '026 '025 '023 '022 '020 '018 '017 '016 '015 '014	19.8 18.9 18.0 17.2 16.3 15.5 14.8 14.1 13.4 12.7 12.1 11.5 10.9 10.4 9.9 9.4	-0'4 0'4 0'4 0'3 0'3 0'3 0'3 0'3 0'2 0'2 0'2 0'2 0'2 0'2	0.0 0.9 1.8 2.6 3.5 4.3 5.7 6.4 7.1 7.7 8.3 8.9 9.4 9.9	+1.0 1.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0	100 95 90 86 82 78 74 71 68 64 61 58 55 52 49	- 5 5 4 4 4 4 4 3 3 3 3 3 3 3 3 2 2	470°5 471°0 471°5 472°0 *4 472°9 473°3 473°7 474°1 *5 474°9 475°2 *5 475°8 476°1 *4	- 0°7	'4 6.5 8.1 '6 9.7 '7 11.3 '8 13.0 '9 14.6
	84 83 82 81 80 79 78 77 76	74'9 73'3 71'7 70'2 68'6 67'0 65'5 63'9 62'4	0°5 0°5 0°5 0°5 0°5 0°5 0°4 0°4 -0°4	0'861 0'818 0'777 0'738 0'700 0'663 0'628 0'594	*013 *013 *012 *012 *012 *011 *011	8.9 8.4 8.0 7.6 7.2 6.8 6.4 6.1 5.8	0.1 0.1 0.1 0.1 0.1 0.1 0.1	10'9 11'4 11'8 12'2 12'6 13'0 13'4 13'7 14'0	0.8 0.8 0.7 0.7 0.7 0.7 0.7 0.7 0.7	47 45 43 40 38 36 34 32 30 29	2 2 2 2 2 2 2 1 1	476.9 477.2 4.6 477.9 478.1 3 478.5		*01 0'2 '02 0'3 '03 0'5 '04 0'7 '05 0'8 '06 1'0 '07 1'1 '08 1'3 '09 1'5

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